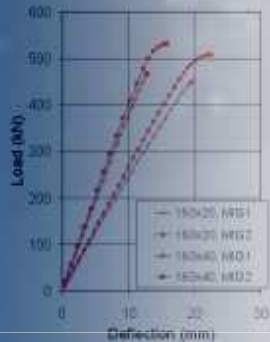


Seismic performance quantification of steel corrugated shear wall system



Laszlo Gergely Vigh, (Geri)

Visiting scholar, Stanford, CA

*Asst. Prof., Budapest University of Technology and Economics,
Dept. Of Structural Engineering, Hungary*

and

Professor Gregory Deierlein,

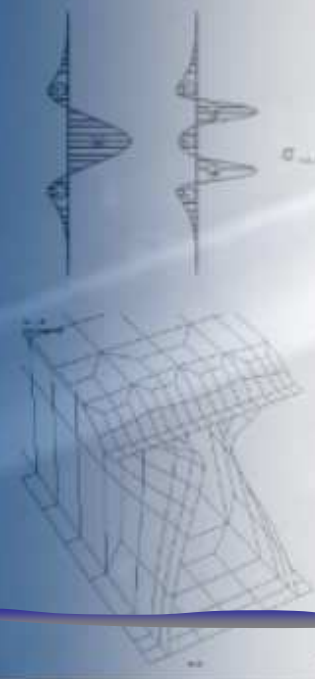
Professor Eduardo Miranda,

Abbie Liel (Stanford)

Stephen Tipping (Tipping Mar + Associates)

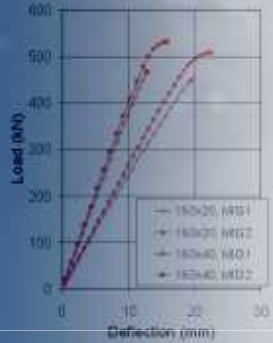
Thanks are due to:

The Thomas Cholnoky Foundation, Inc.



Little background...

- Hard to work at Dept. of Structural Engineering

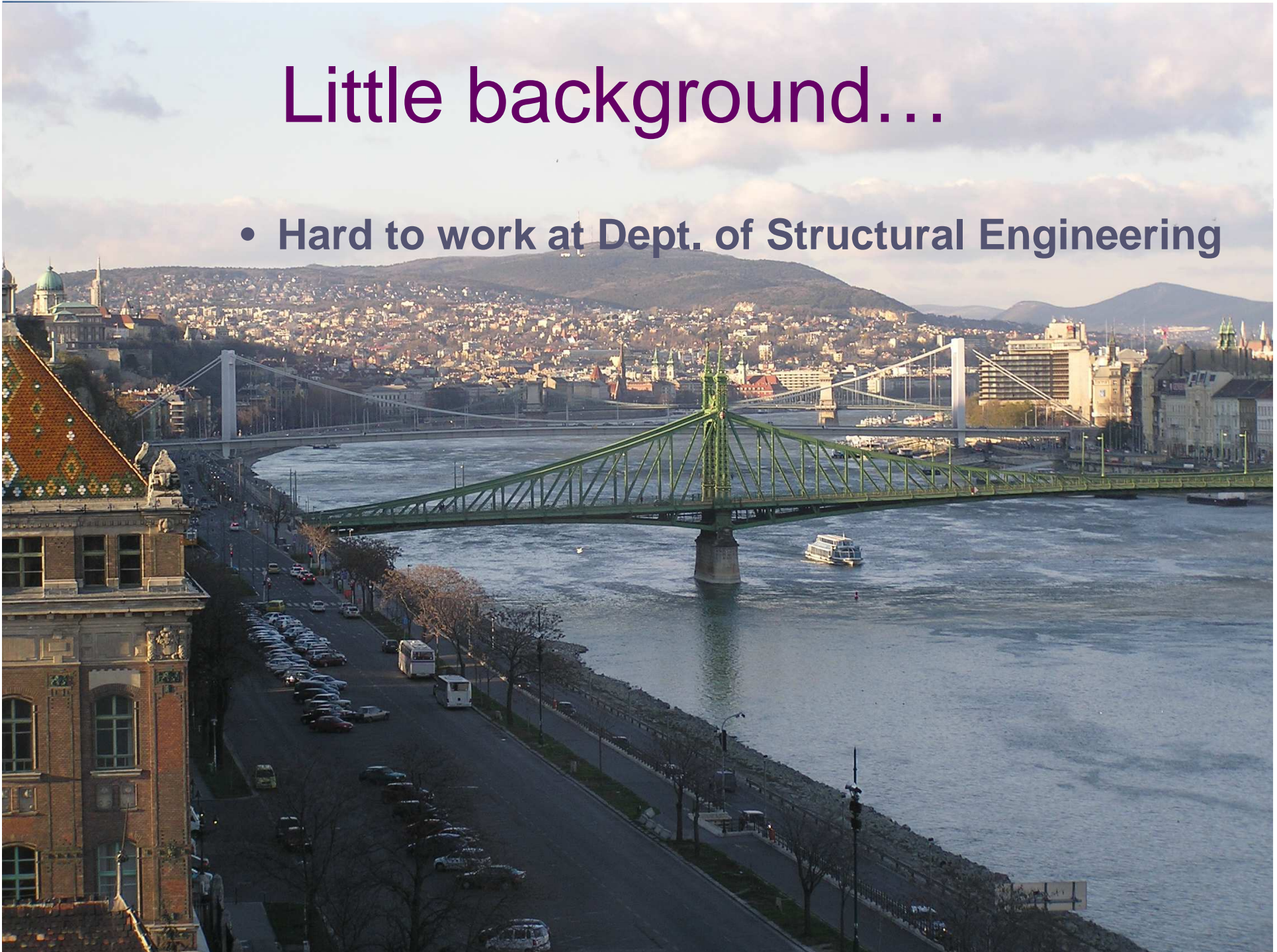


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Little background...

- Hard to work at Dept. of Structural Engineering



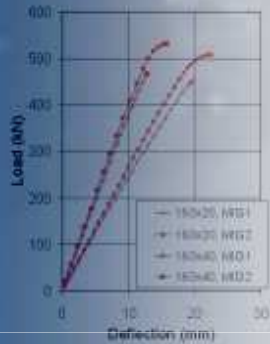
Little background...

- Hard to work at Dept. of Structural Engineering



Little background...

- Budapest University of Technology and Economics



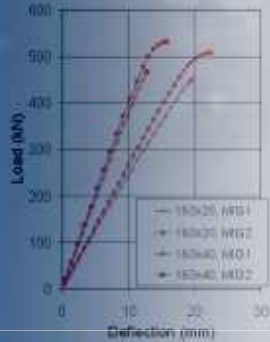
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Source: www.bme.hu

Little background...

- Budapest University of Technology and Economics

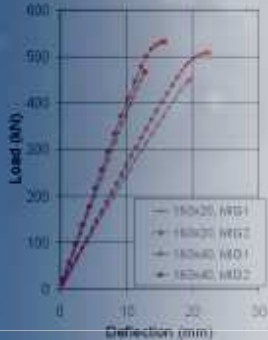


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Little background...

- Budapest University of Technology and Economics:
 - 8 faculties and several innovation centers
 - **Faculty of Civil Engineering:**
 - 10 departments
 - Dept. of Structural Engineering:
 - staffs: 57 (incl. appr. 25 of asst. prof – prof)
 - 22 BSc, 16 MSc courses + optionals



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Little background...

- **Dept. of Structural Engineering**

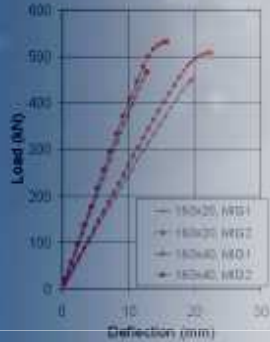
- 1. Education**

- 2. Research – national research funds, and ‘selfish’ researches**

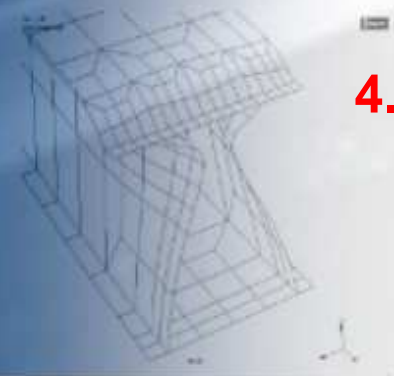
- 3. Industry & University**

- **R&D**
- **Co-designer**
- **Expert**
- **Independent checks**
- **Laboratory and site testing – Accredited laboratory**

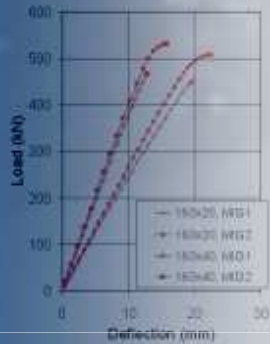
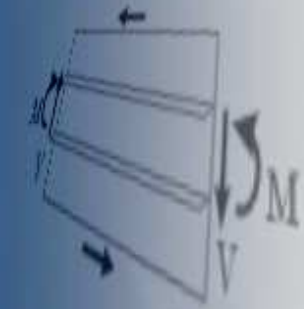
- 4. Student life...**



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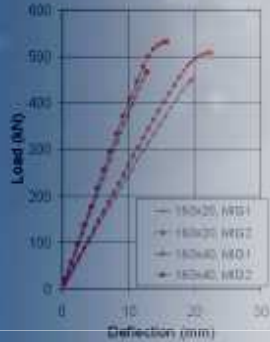
Seismic performance quantification of steel corrugated shear wall systems



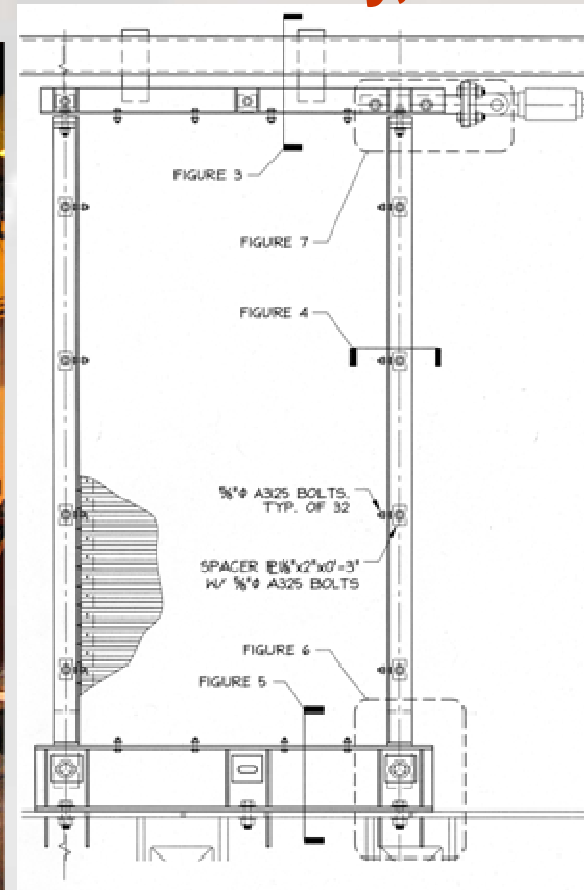
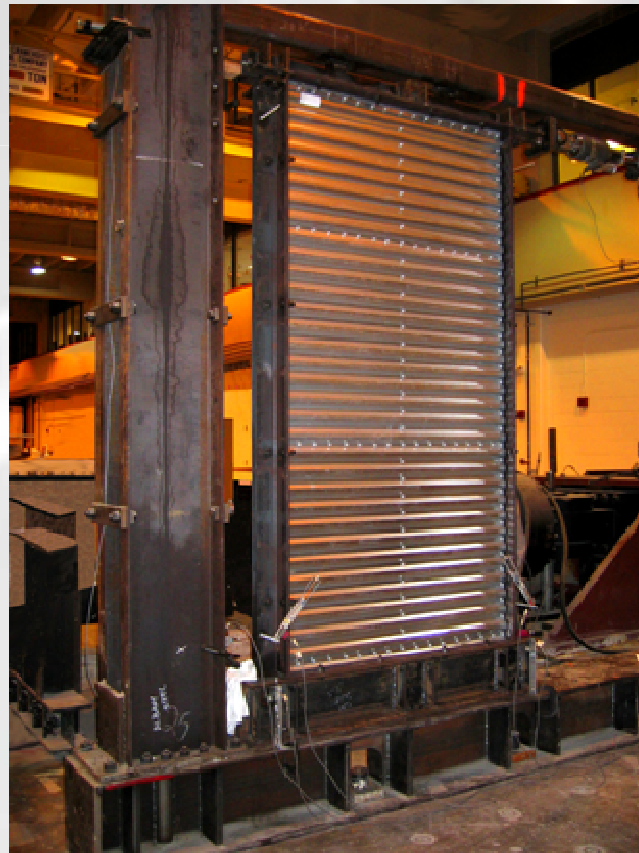
Shear wall system

- corrugated sheet
- boundary elements
- screwed connection

**Tipping Mar and Associates,
Berkeley, CA**



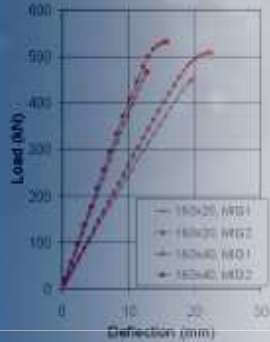
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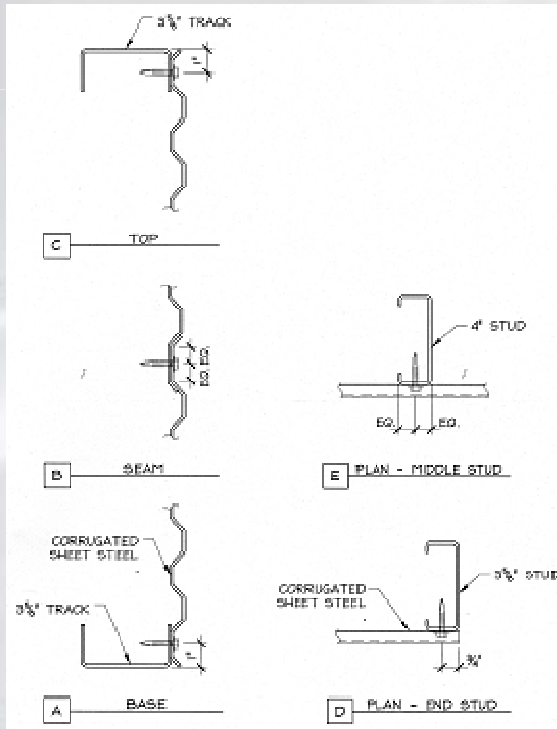
Shear wall system

- corrugated sheet
- boundary elements
- screwed connection

Assembly	stud gauge	20	18	16	16
	screw size	12	12	12	14
sheathing	screw spacing	Group #			
22	6"	1	25	7	
22	3"	3	6	8	
18	3"		13	14	16



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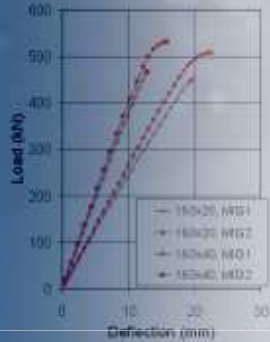


Seismic performance quantification by ATC-63

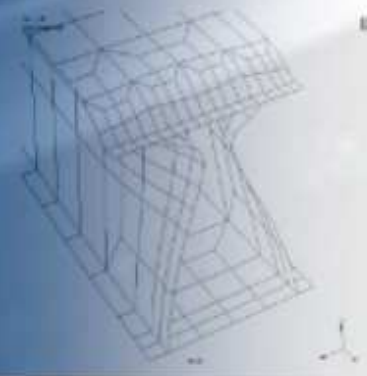
- performance quantification by cyclic tests
or
- Applied Technology Council, Project 63
- achieves primary life safety performance objective by requiring an acceptably low probability of collapse
- R , Ω_0 , C_d factors

- 1) idealized archetypical systems: realization, design (assume R)
- 2) analytical model development and calibration
- 3) nonlinear static (pushover) analysis $\rightarrow \Omega_0$
- 4) nonlinear incremental dynamic analysis (IDA)
- 5) fragility curves;
adjusted collapse margin ratio (ACMR) vs. acceptable ACMR

↓
 R , C_d

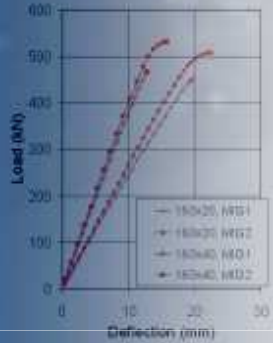


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Experimental results

- Stojadinovic et al. at UC Berkeley
- 44 specimens

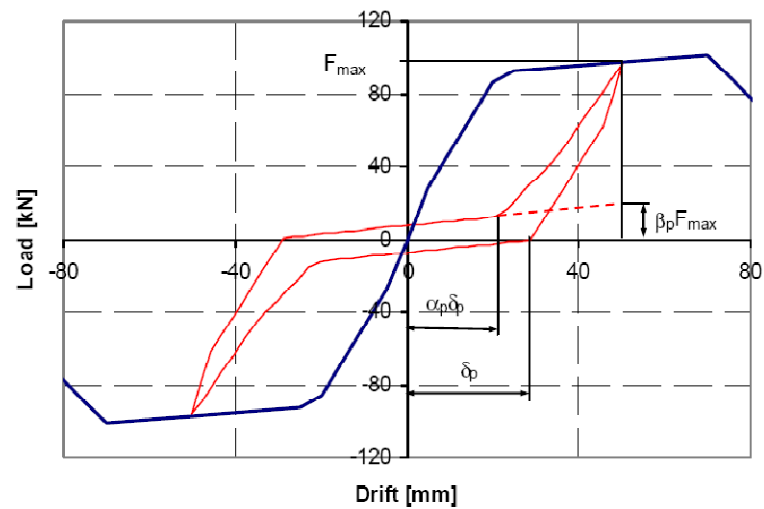
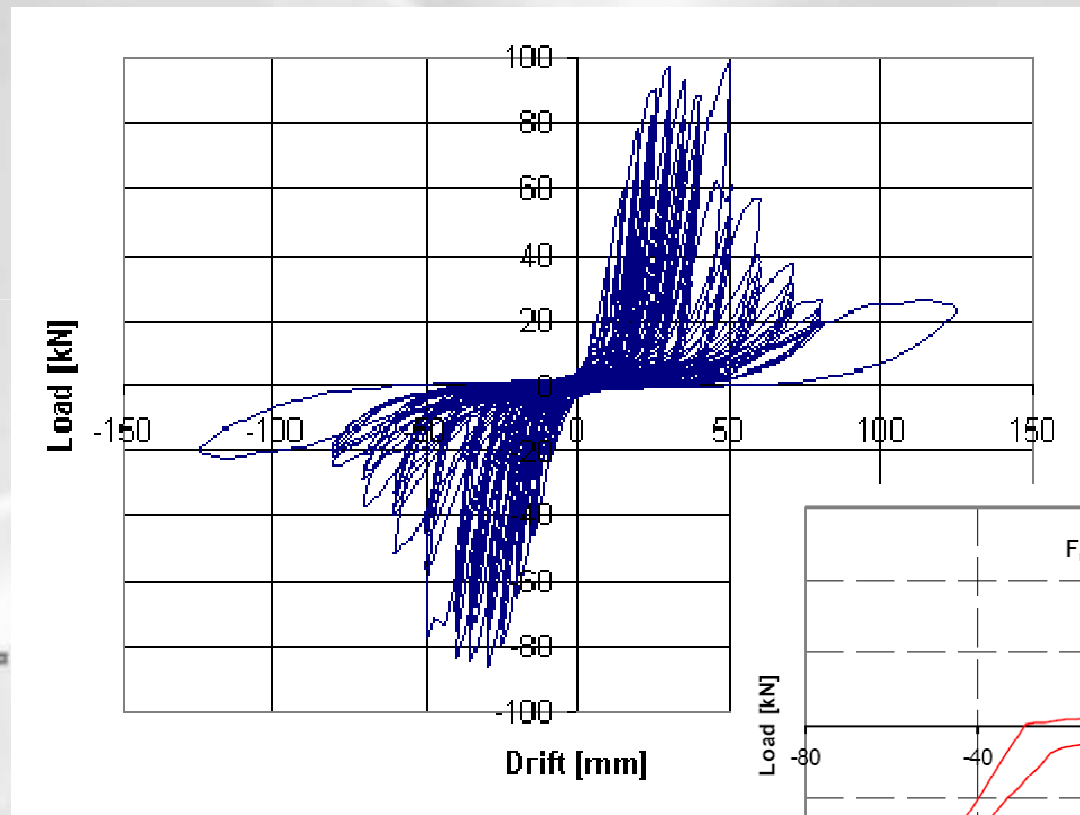
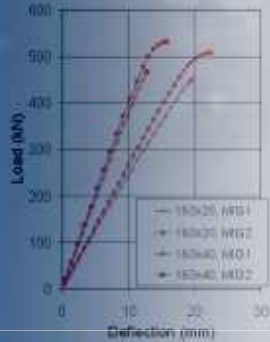


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Experimental results

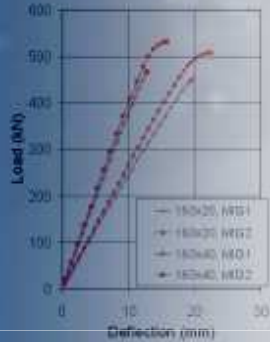
- pinching hysteresis behavior



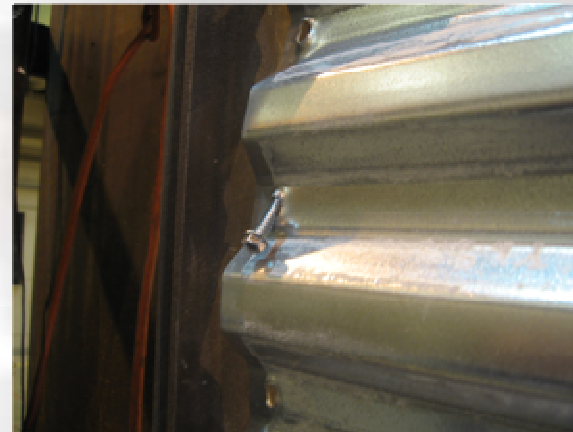
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Experimental results

- failure modes



a) bearing



b) screw pull-out / tilt



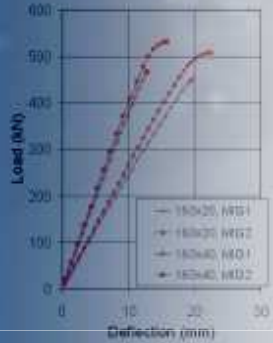
c) buckling and warping of corrugated sheet after screw pull-out

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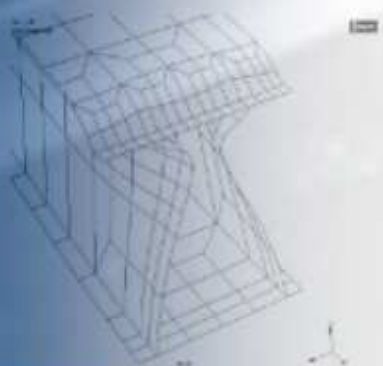


Experimental results

- failure modes

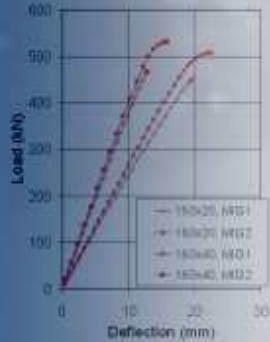


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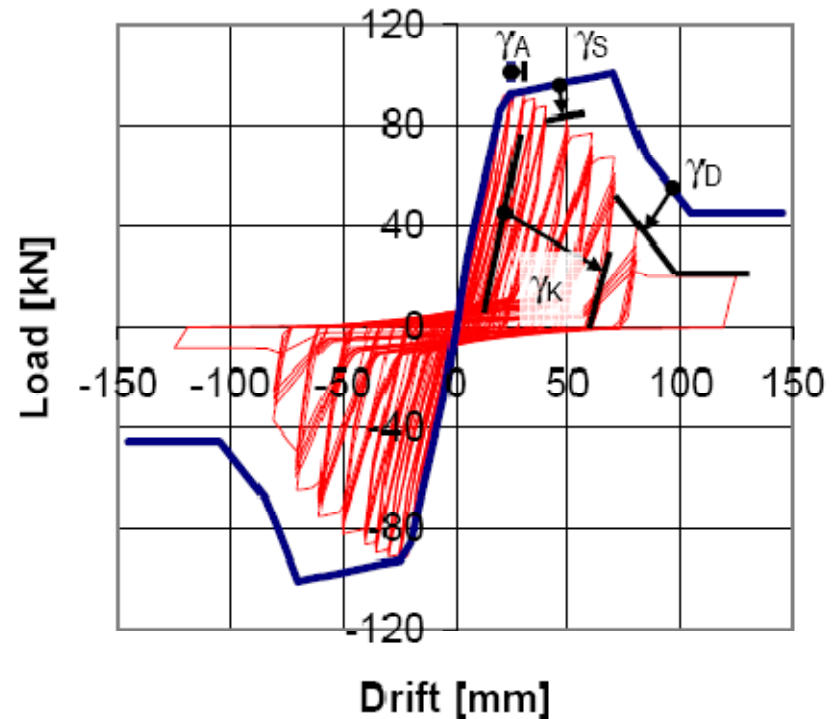
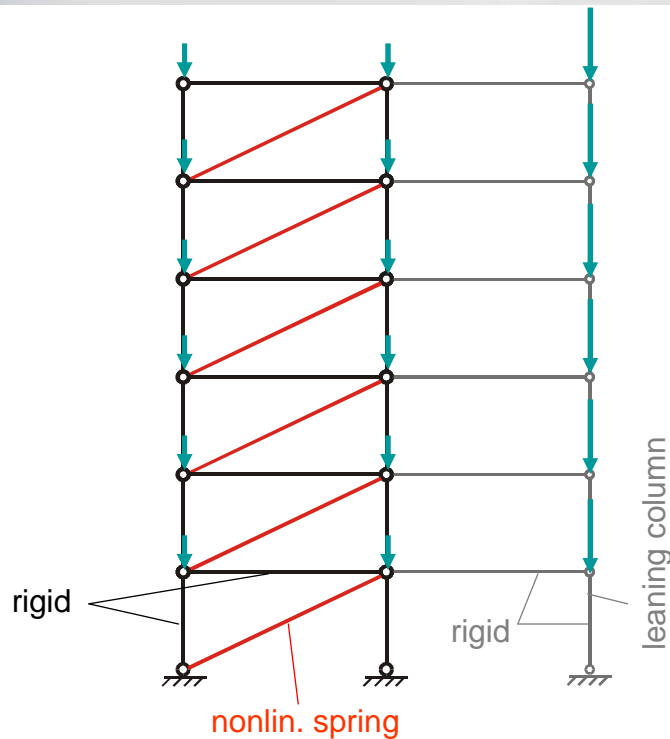


Shear wall behavior – estimation of monotonic backbone curve

- challenge:
 - cyclic behavior is path-dependent
 - calibration to test results – we should know the monotonic behavior

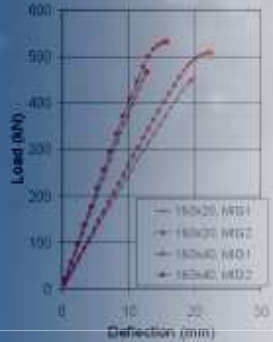


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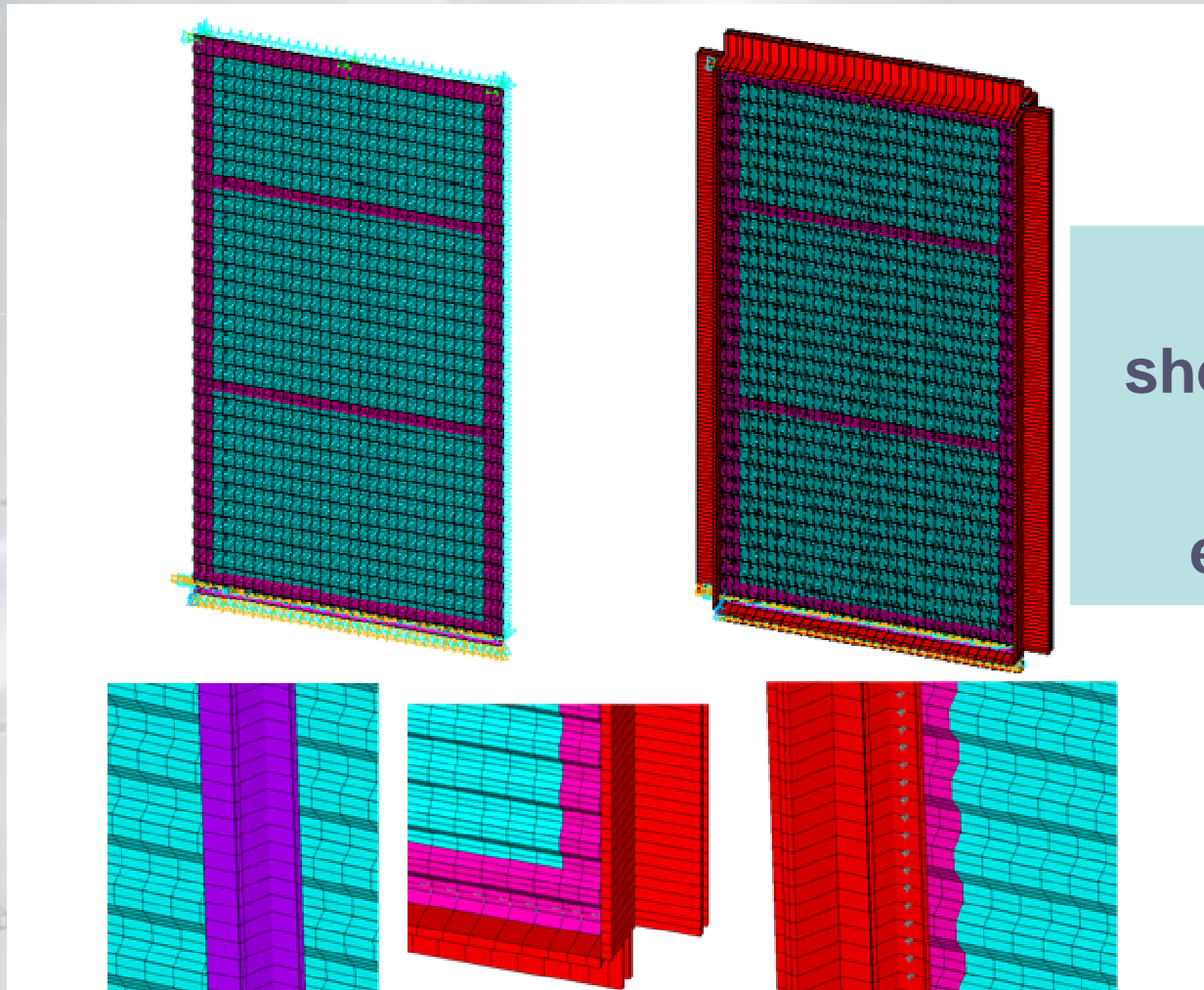


Shear wall behavior – estimation of monotonic backbone curve

- modelling technique



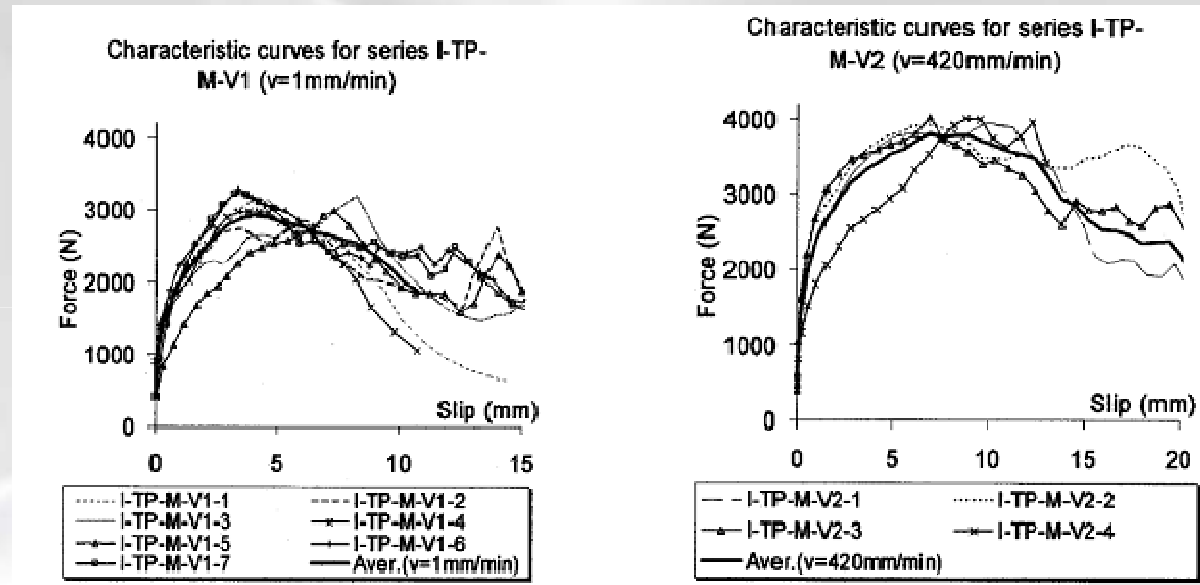
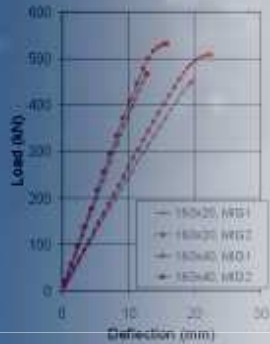
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ANSYS
shell, beam &
spring
elements

Shear wall behavior – estimation of monotonic backbone curve

- single screw connection behavior



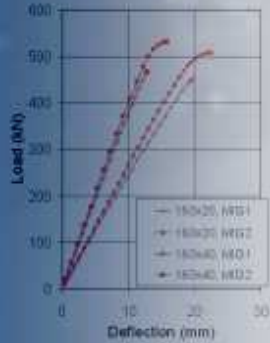
Source: Dubina et al.

- literature
- EC3
- published experimental data

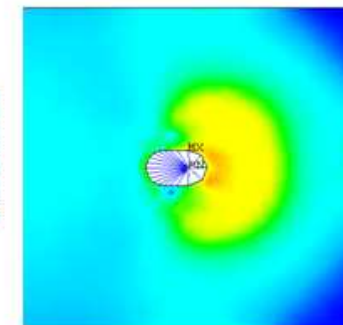
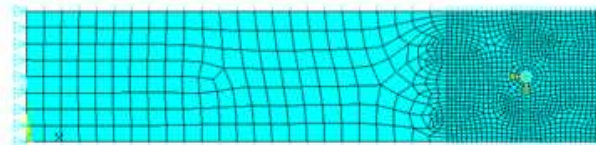
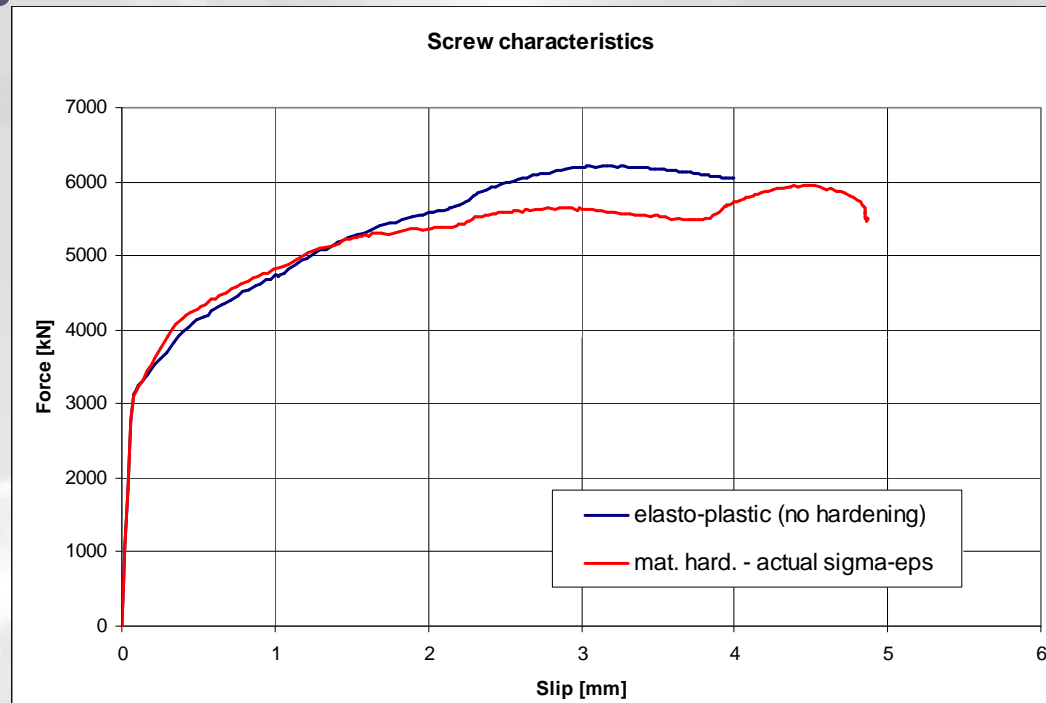
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Shear wall behavior – estimation of monotonic backbone curve

- single screw connection behavior

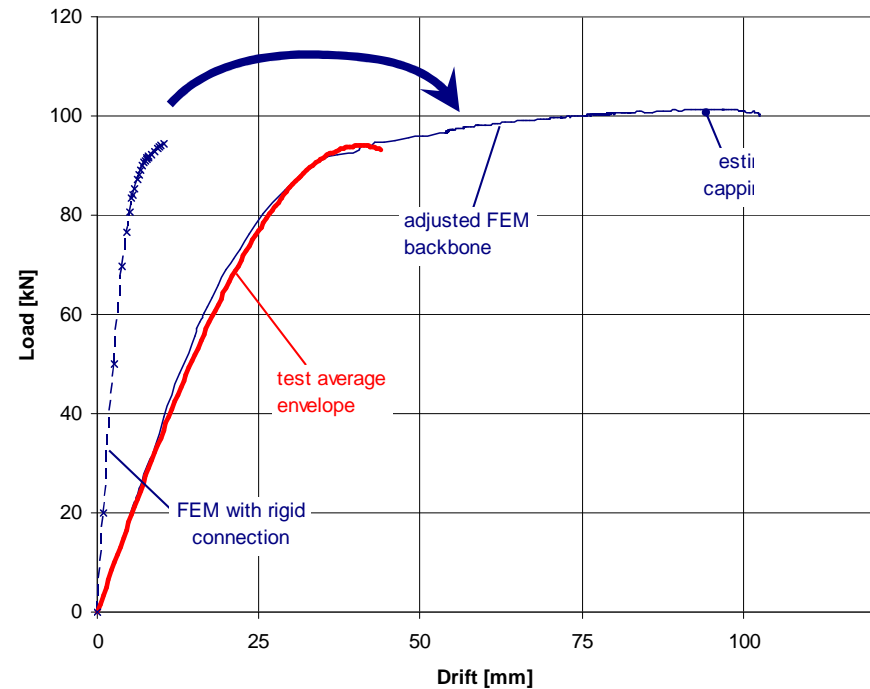
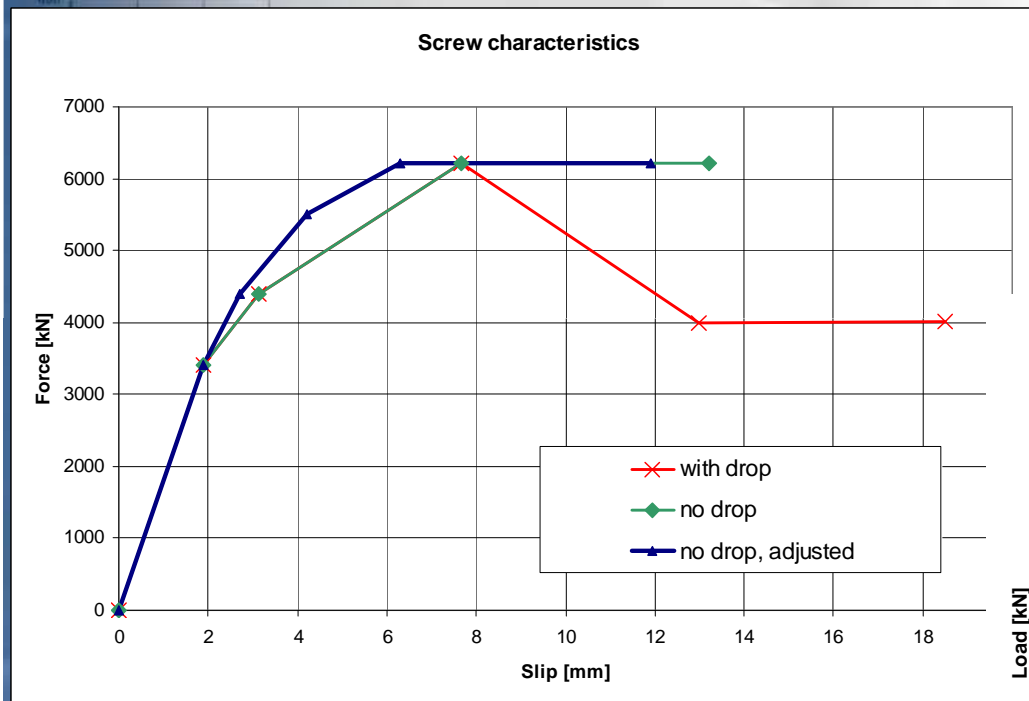


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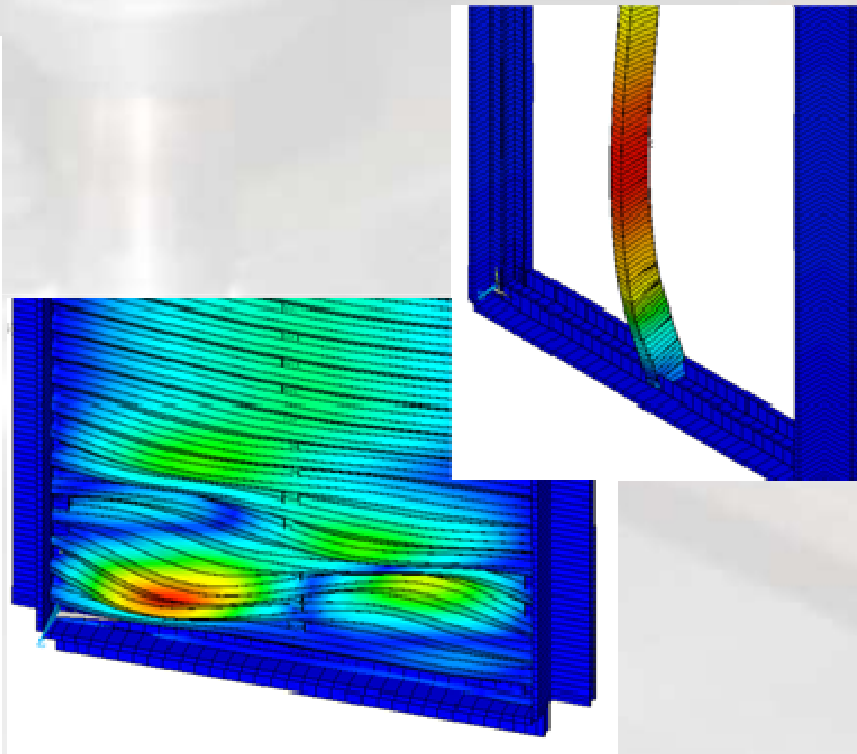
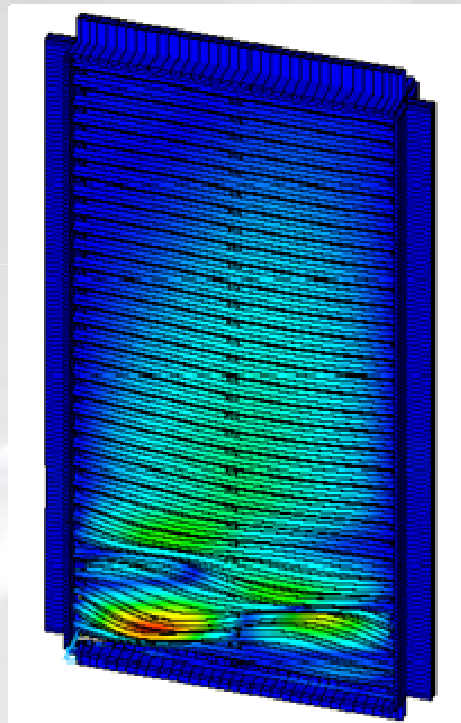
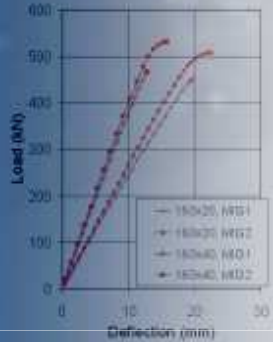
Shear wall behavior – estimation of monotonic backbone curve

- single screw connection behavior



Shear wall behavior – estimation of monotonic backbone curve

- analysis of tested shear walls

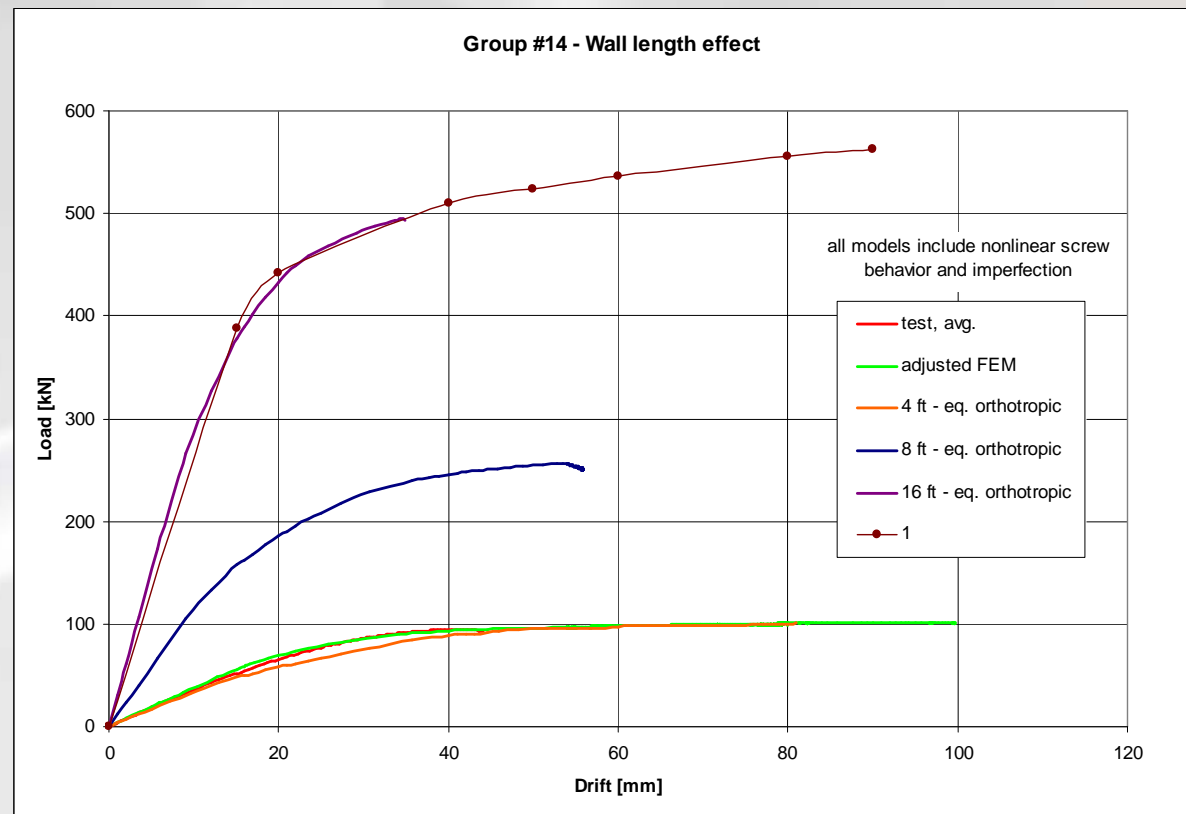
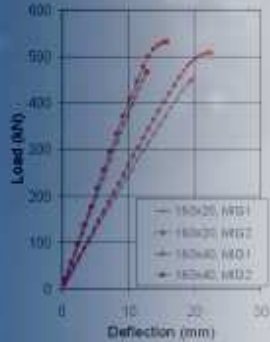


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Shear wall behavior – estimation of monotonic backbone curve

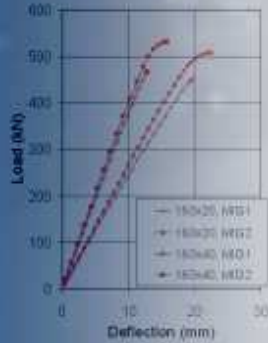
- extension to longer walls



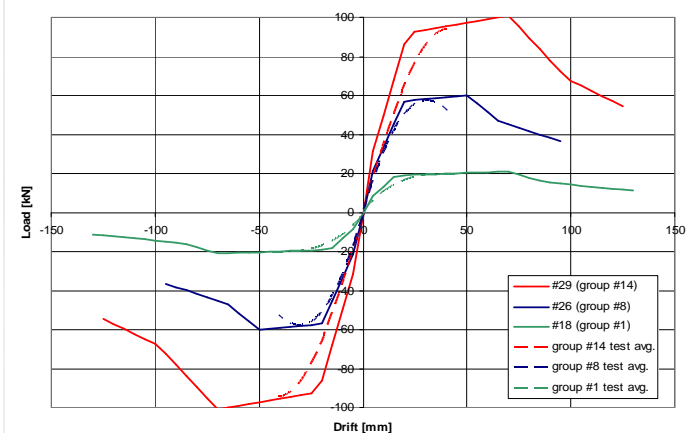
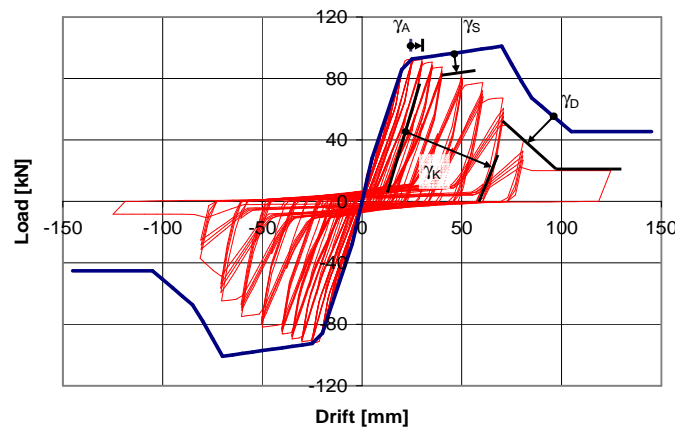
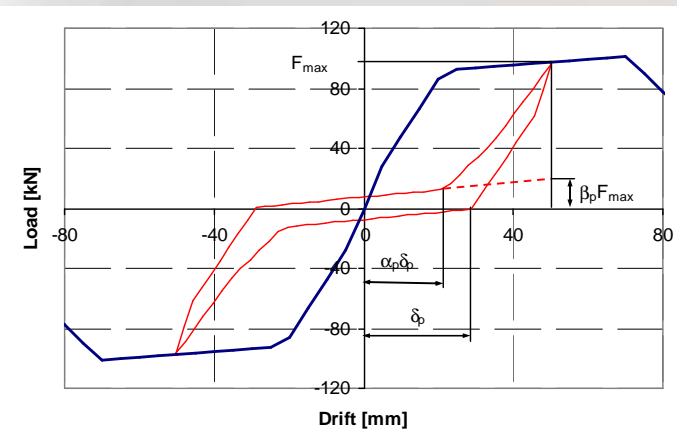
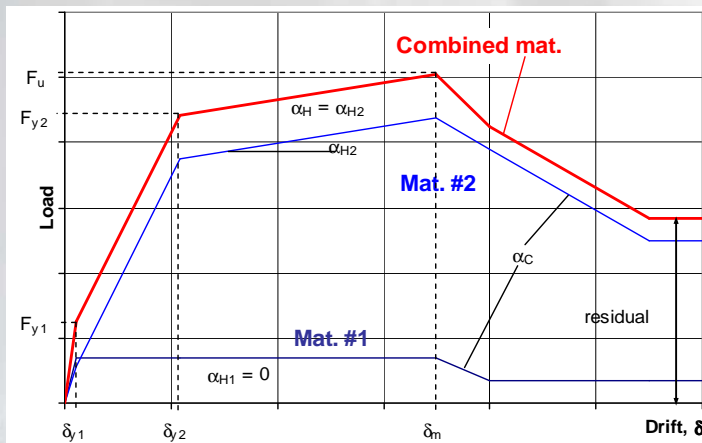
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Model calibration

- OpenSees
- Ibarra – Medina – Krawinkler model

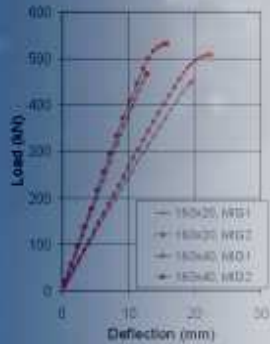


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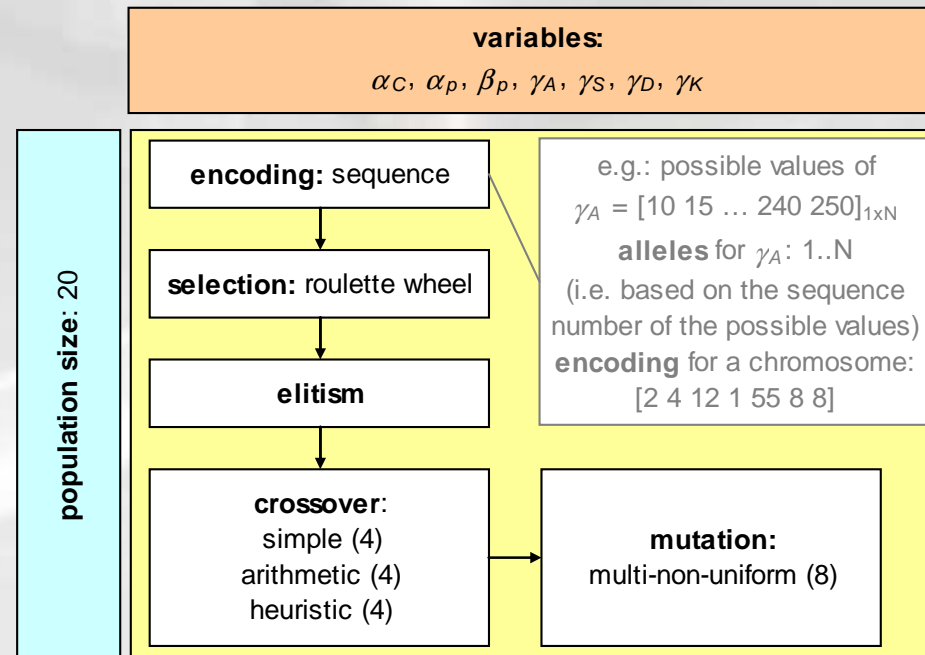


Model calibration

- calibration: GA

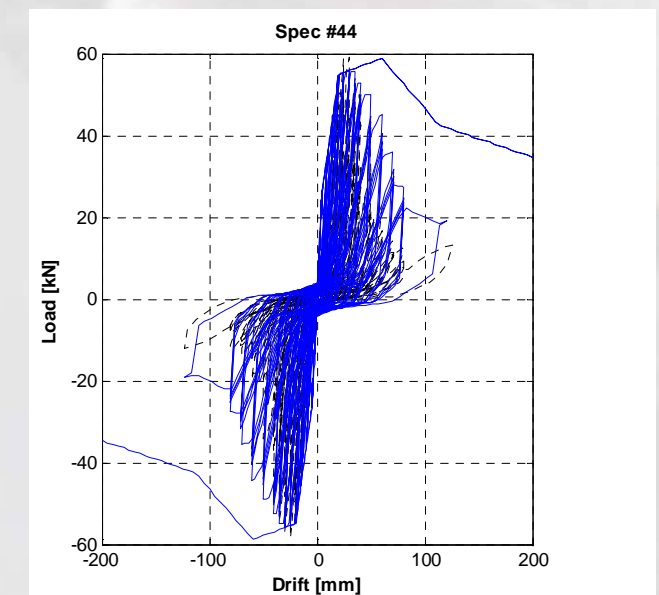
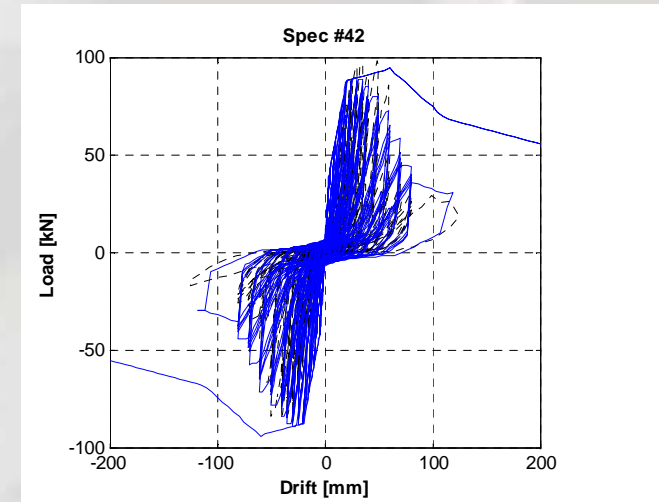
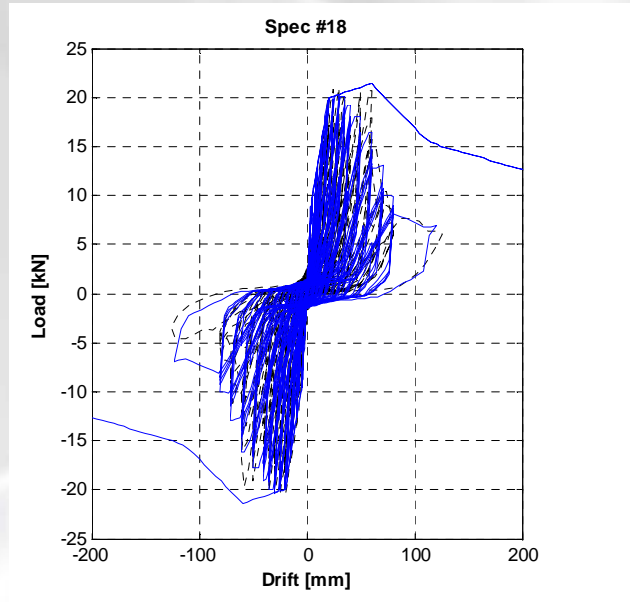
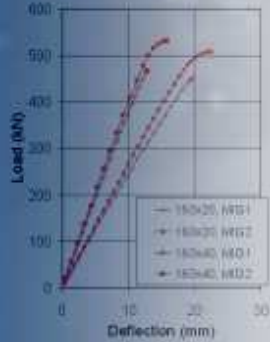


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Model calibration

- final – uniform – model

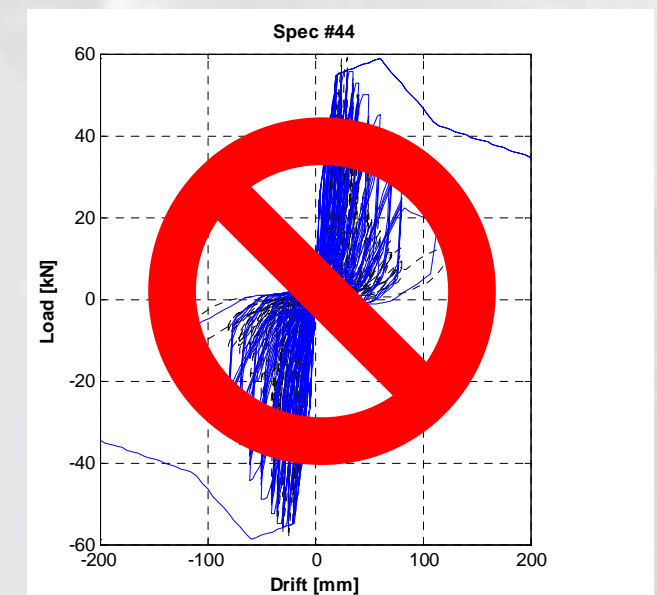
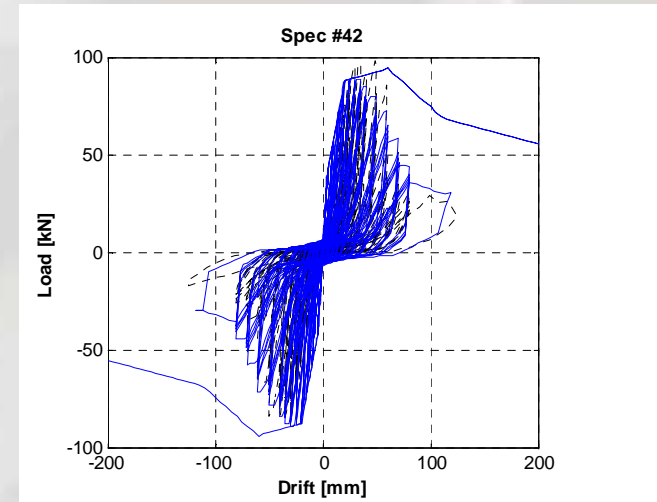
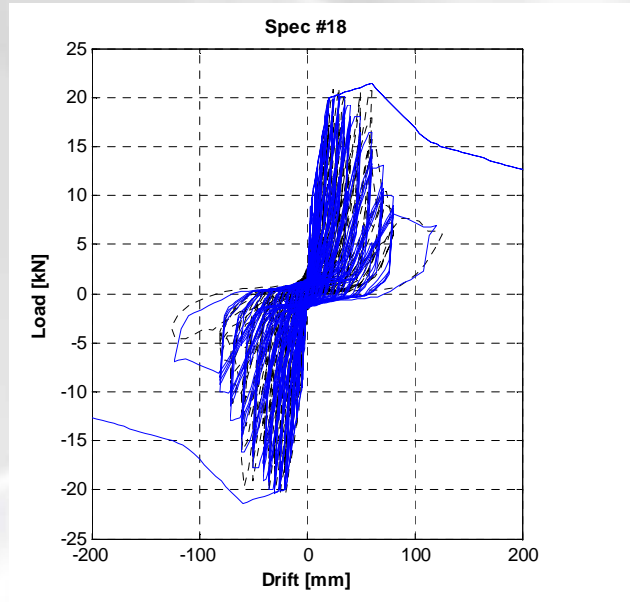
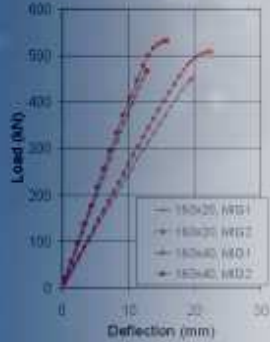


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Assembly	stud gauge	20	18	18	18
	screw size	12	12	12	14
sheathing	screw spacing	Group #			
22	6"	1	25	7	
22	3"	3	6	8	
18	3"		13	14	16

Model calibration

- final – uniform – model



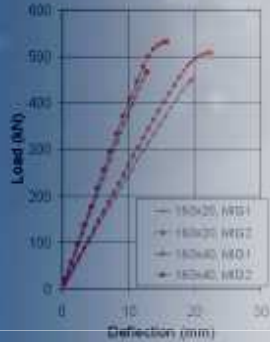
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Building archetypes

- Archetype definitions

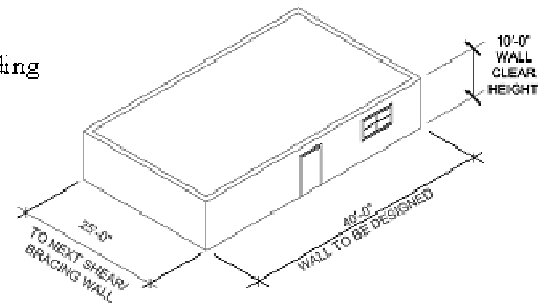
- building function, configurations
- number of stories
- seismic zone



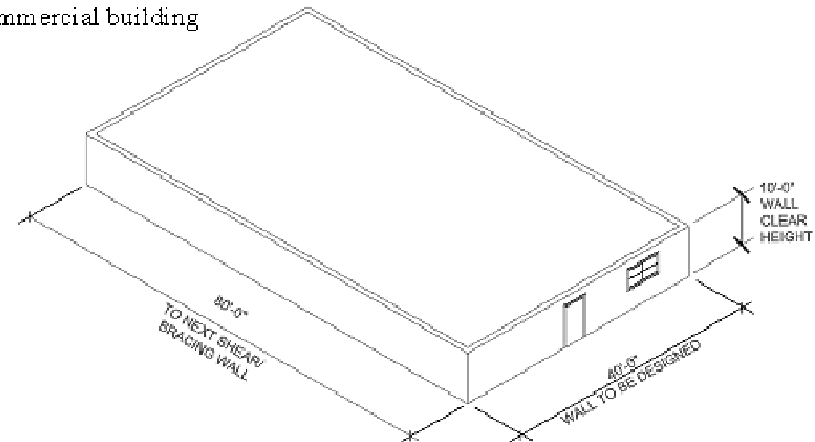
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a) residential building



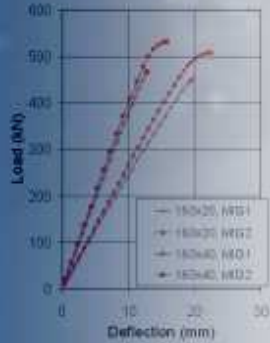
b) commercial building



Building archetypes

- Archetype definitions

R = 4 High seismic (SDC Dmax)
 $S_S = 1.5, S_1 = 0.9$ ($S_{DS} = 1.0, S_{D1} = 0.6$)



Archetype	Story #	Function	A_{floor} [sqft]	seismic weight [psf]	Appr. period [s]	Upper limit of period [s]	S_{MT} (at T_a) [g]	C_s [-]	Design base shear [kip]	wall length [ft]
1	1	Commercial	1600	30	0.112	0.16	1.50	0.25	12	12
5	2	Commercial	1600	30	0.19	0.27	1.50	0.25	24	24
9	3	Commercial	1600	30	0.26	0.36	1.50	0.25	36	20

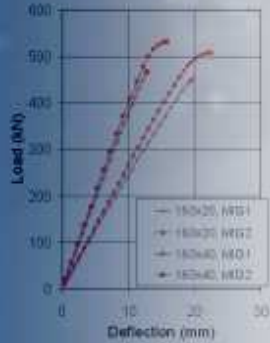
2	1	1&2 Family	500	10	0.112	0.16	1.50	0.25	1.25	8
6	2	1&2 Family	500	10	0.19	0.27	1.50	0.25	2.5	8
10	3	Multi-Family	500	30	0.26	0.36	1.50	0.25	11.25	12
13	4	Multi-Family	500	30	0.32	0.45	1.50	0.25	15	16
15	5	Multi-Family	500	30	0.38	0.53	1.50	0.25	18.75	20

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Building archetypes

- seismic design

- based on assumed R
- simplified proc: equivalent static loading



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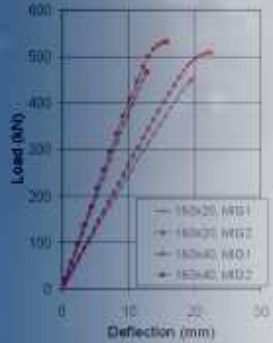


Story	EQ loading [kip]	demand, V_u		wall type (group#)	V_{nom} [plf]	V_{ASD} [plf]	V_{LRFD} [plf]
		[lbs]	[plf]				
R	6250 lbs	6250	312	1	1173	469	657
4	5000	11250	563	1	1173	469	657
3	3750	15000	750	25	1505	602	843
2	2500	17500	875	7	1836	734	1028
1	1250	18750	937	7	1836	734	1028

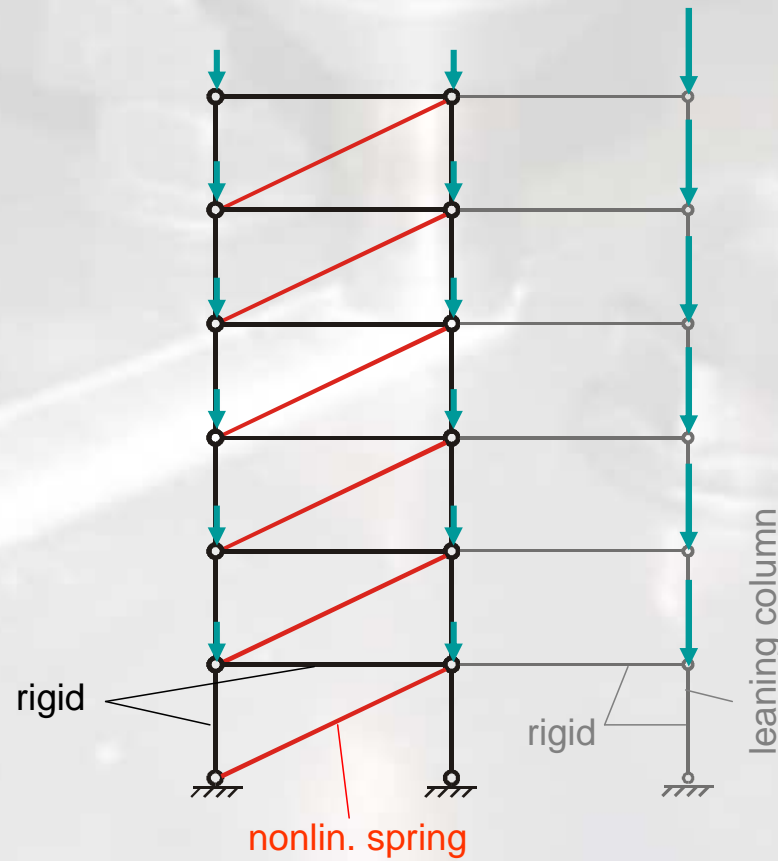


Analytical model

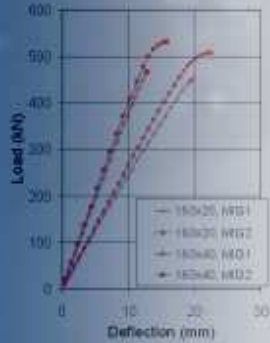
- 2D truss structure



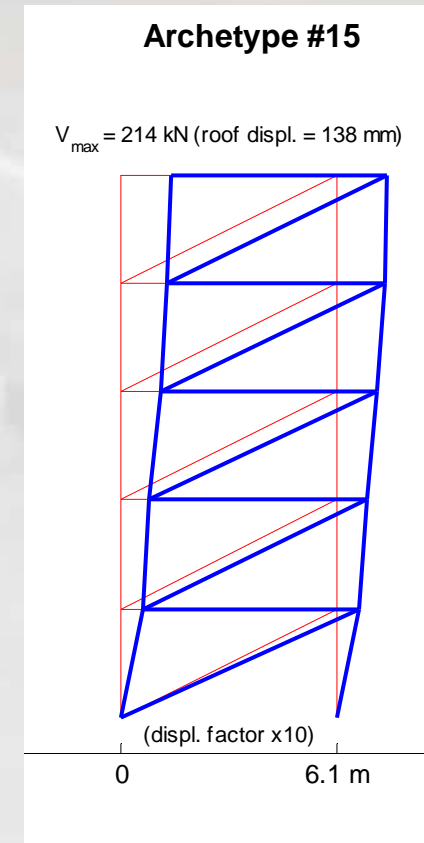
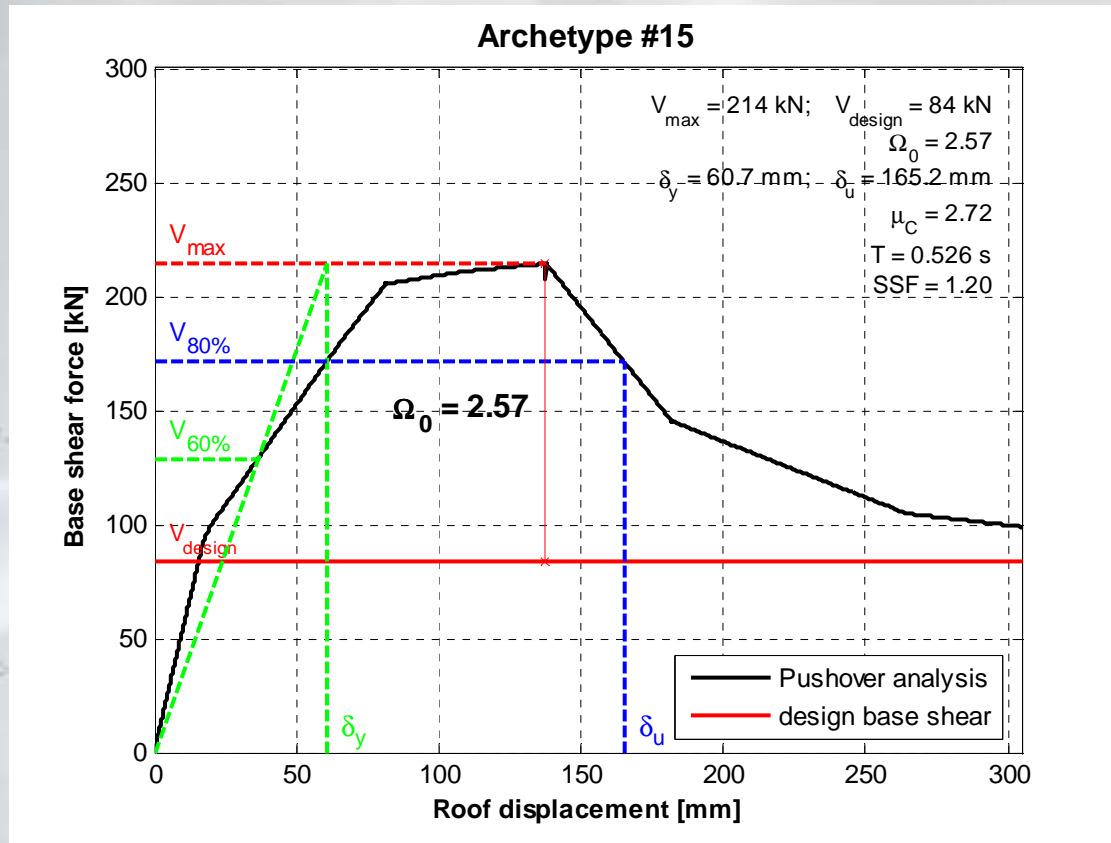
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Pushover analysis

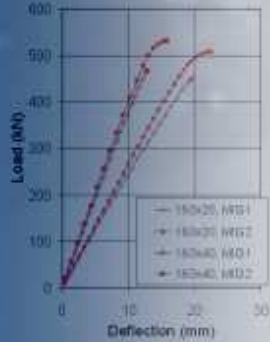


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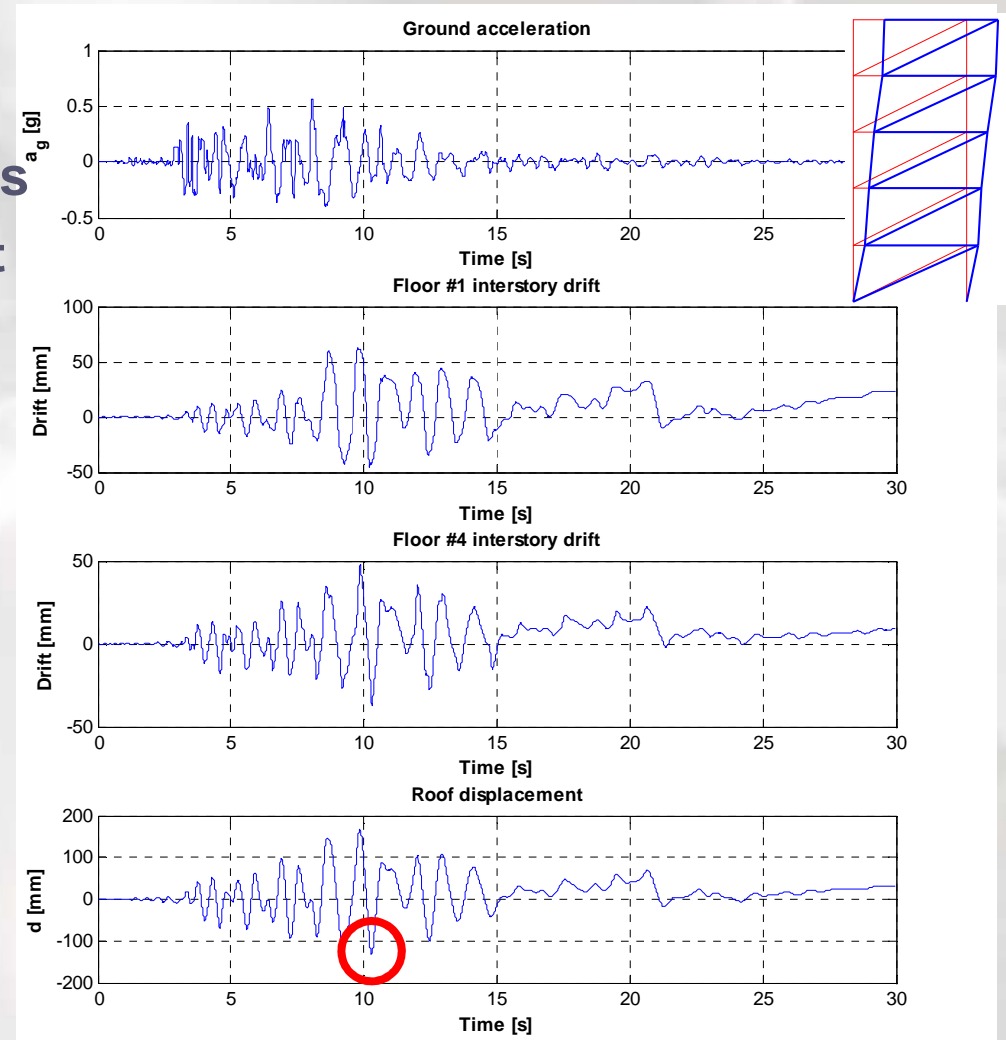


IDA analysis

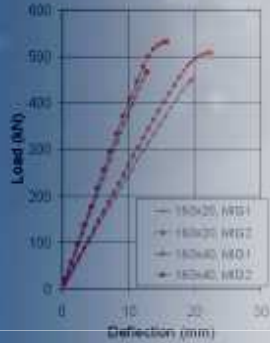
- each archetype
- 44 EQ records
- nonlin. dyn. analysis
- max. interstory drift



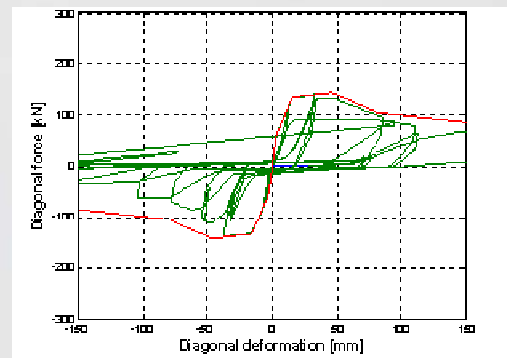
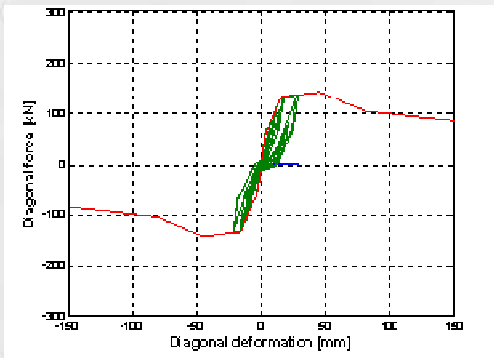
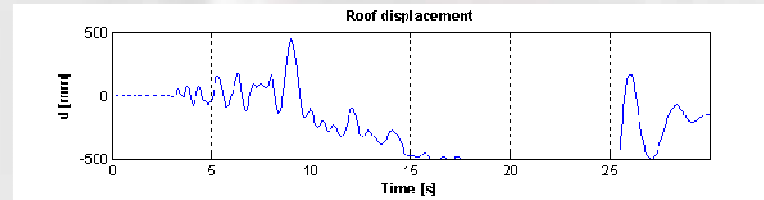
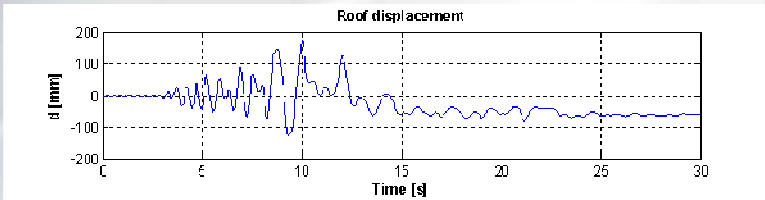
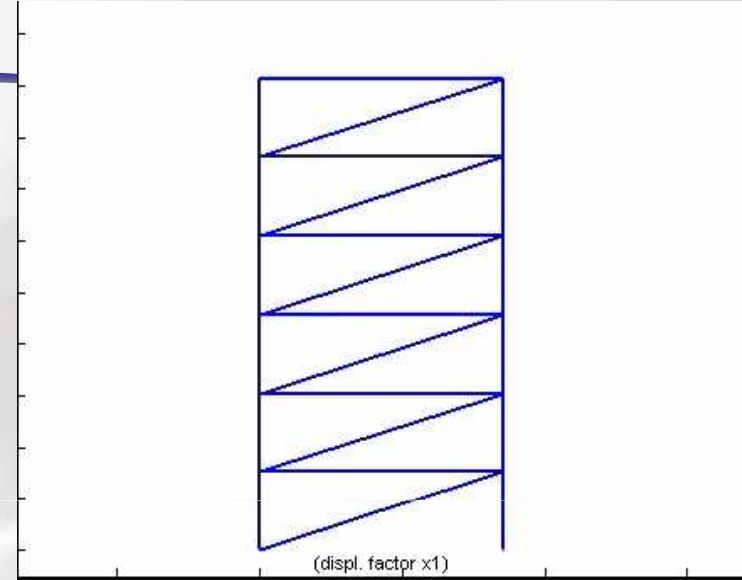
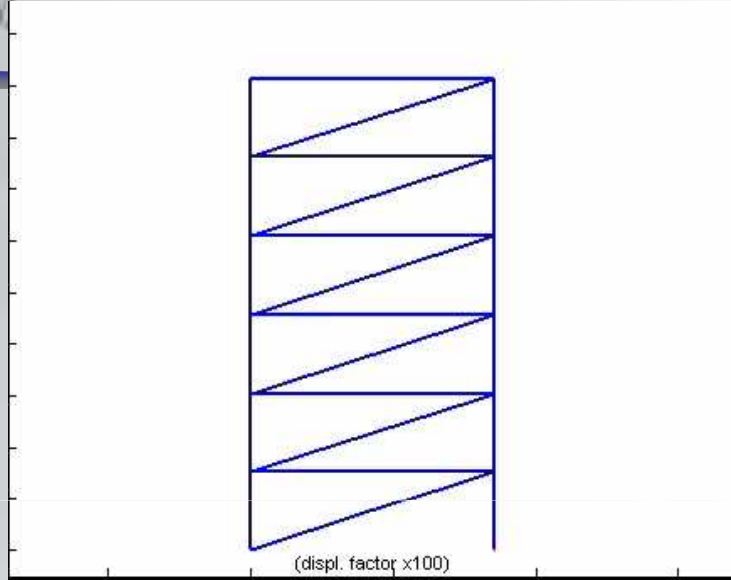
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IDA analysis

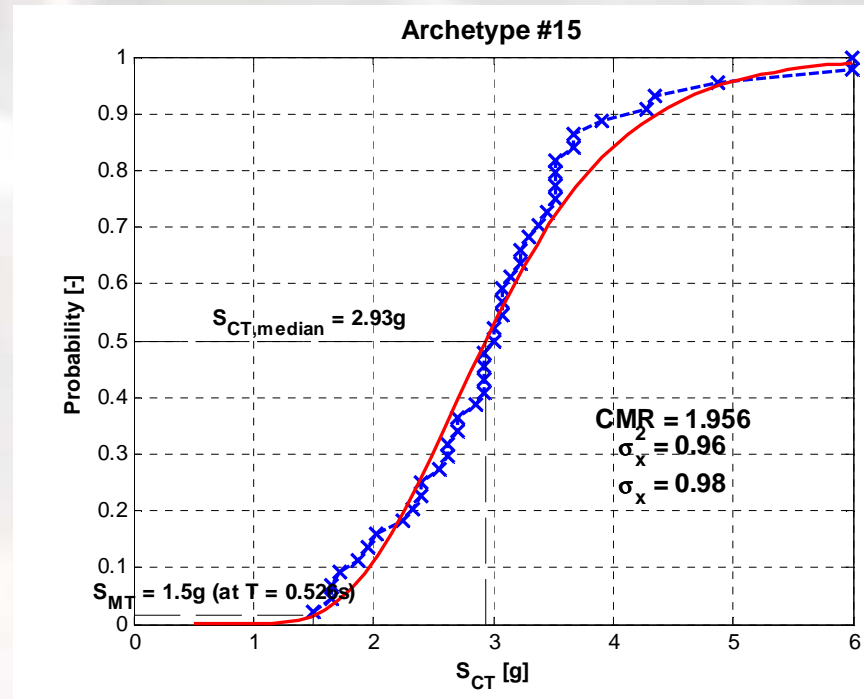
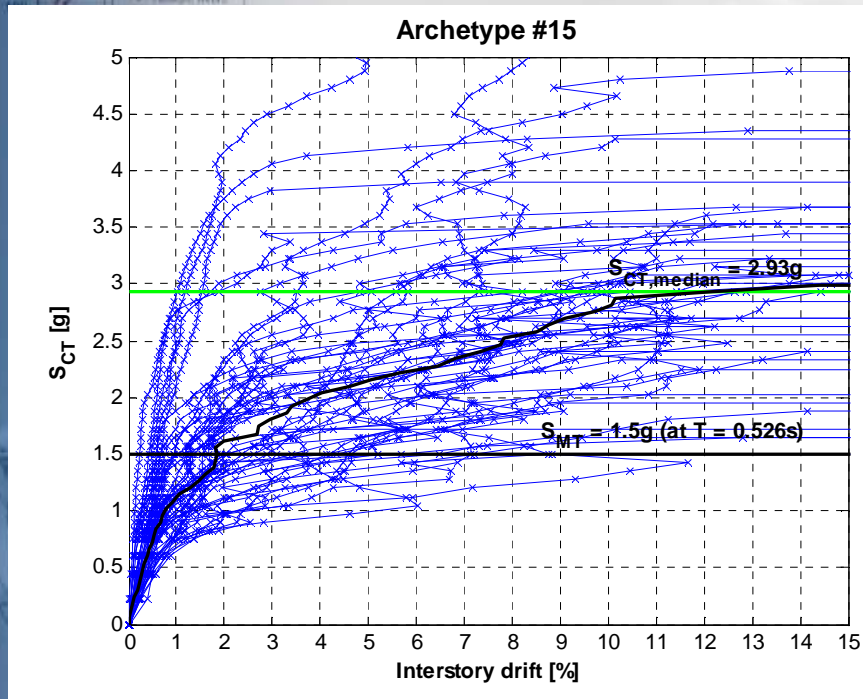


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IDA analysis

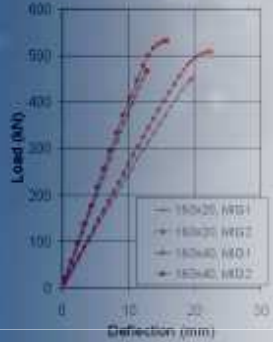
- each archetype
- each record
- scaled up to collapse



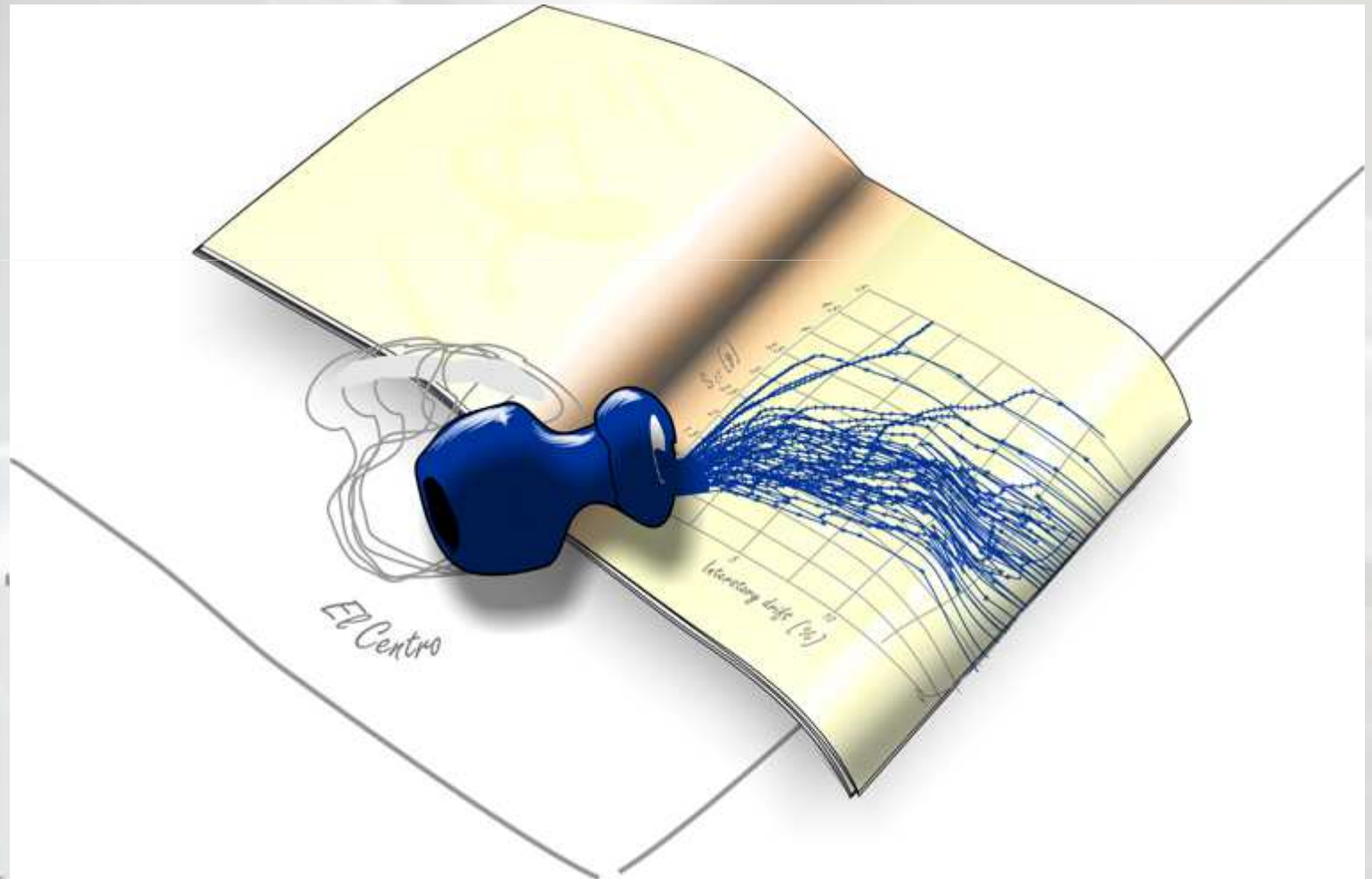
(adjusted) collapse margin ratio

IDA analysis

- or...

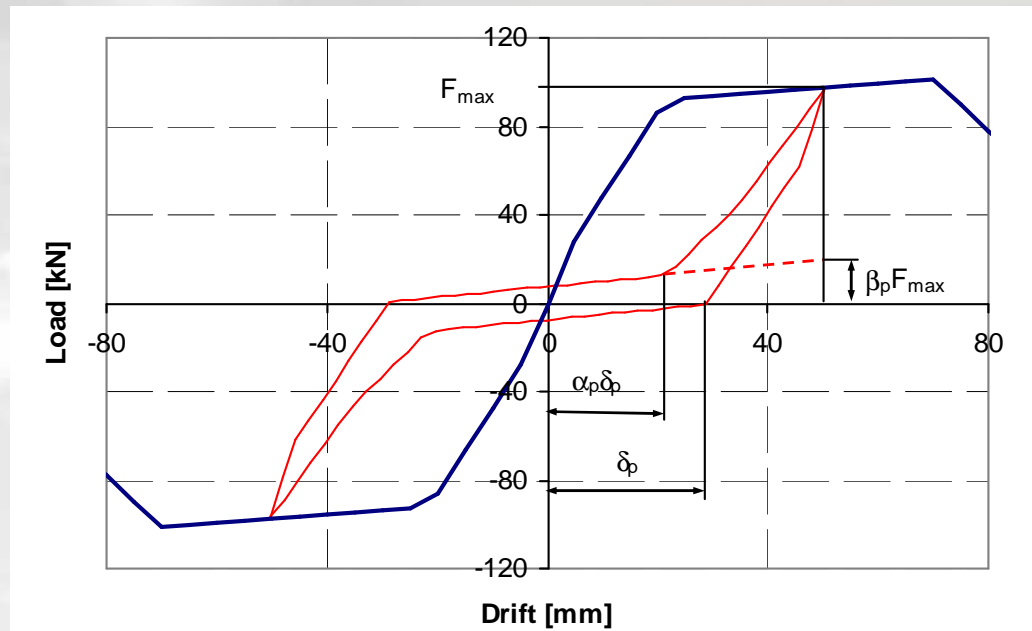
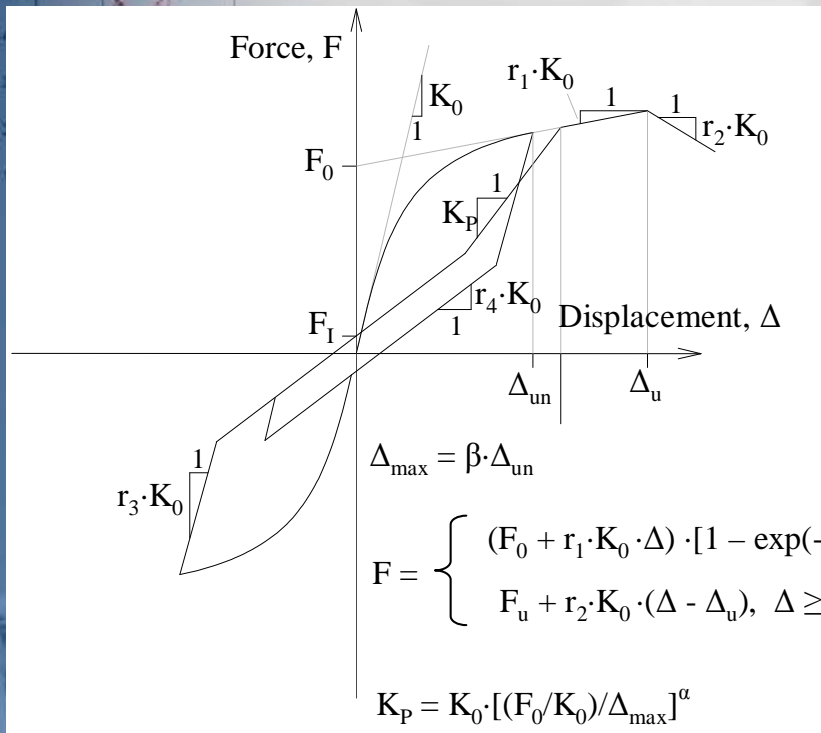


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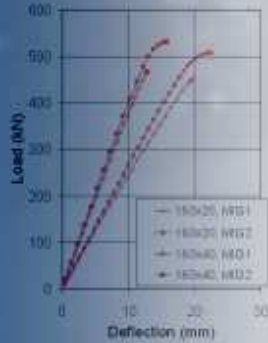
Discussion

- comparison to wooden shear wall

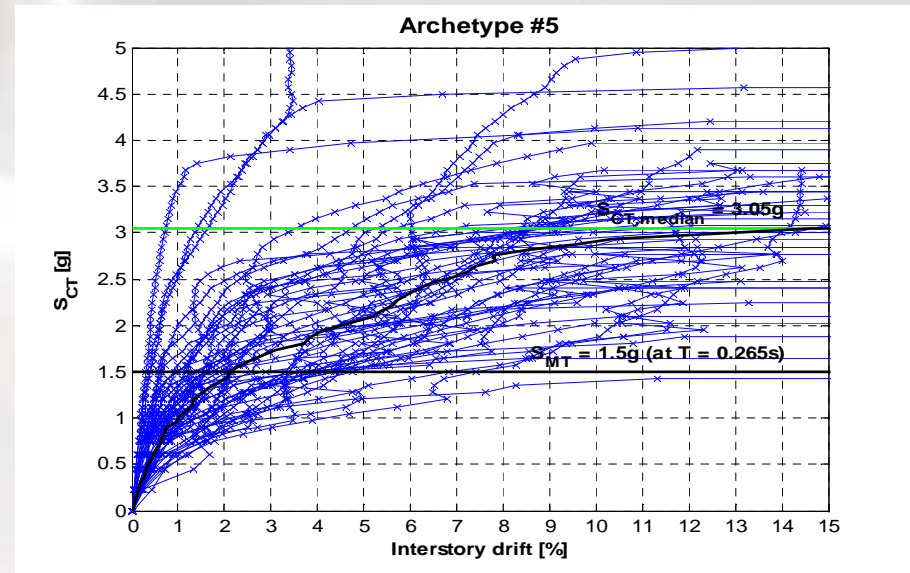
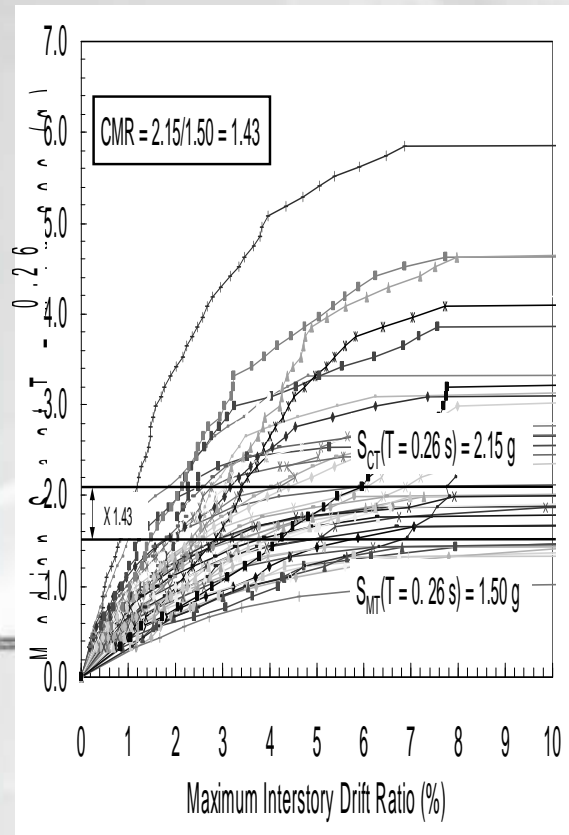


Discussion

- comparison to wooden shear wall



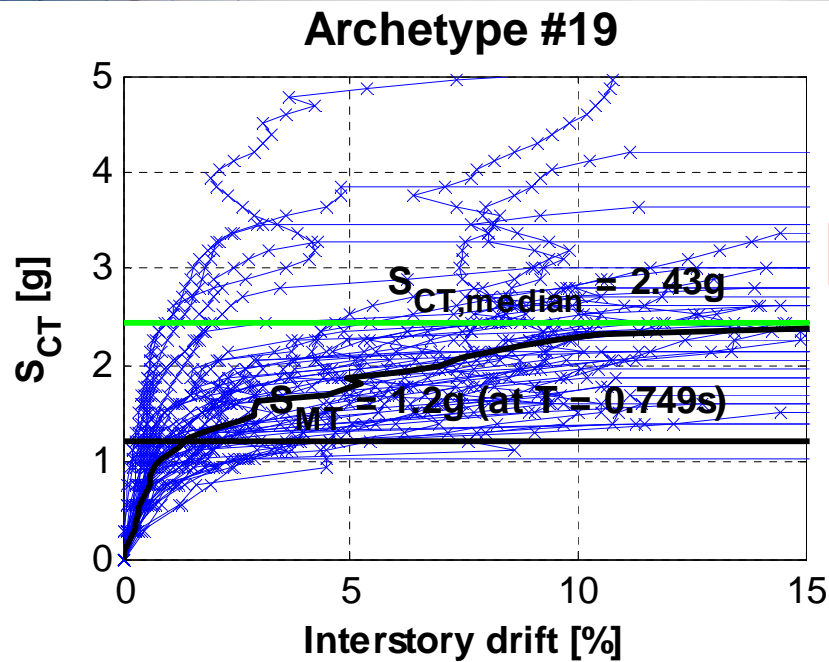
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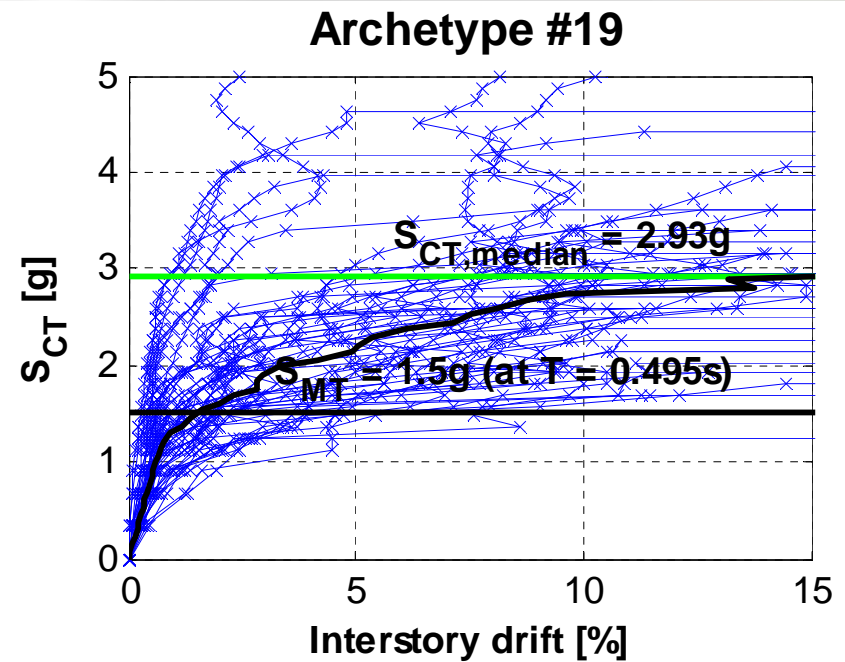
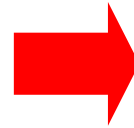
- in general, very similar results

Further observations

- Effect of 'scaling' fundamental period



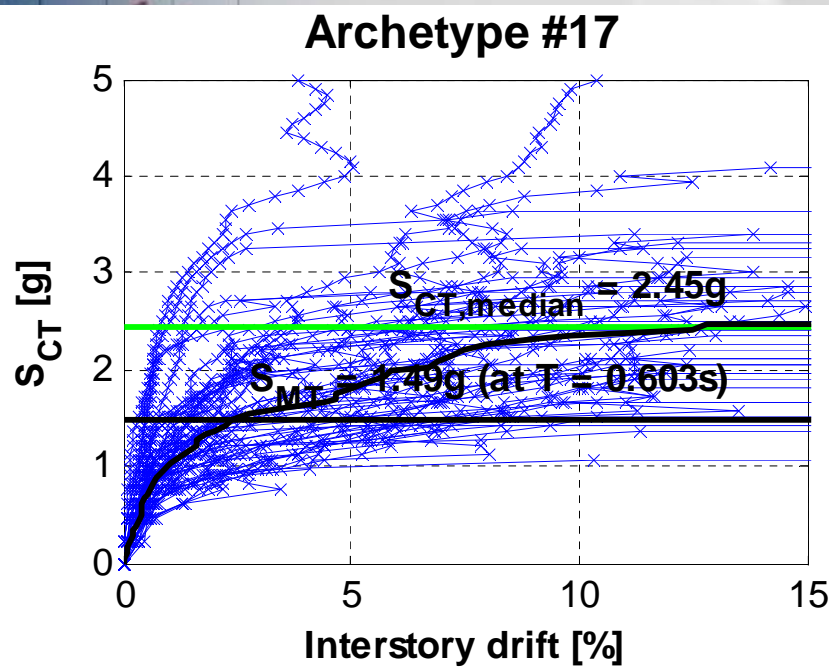
a) scaled at $T_{upper} = 0.749$ s



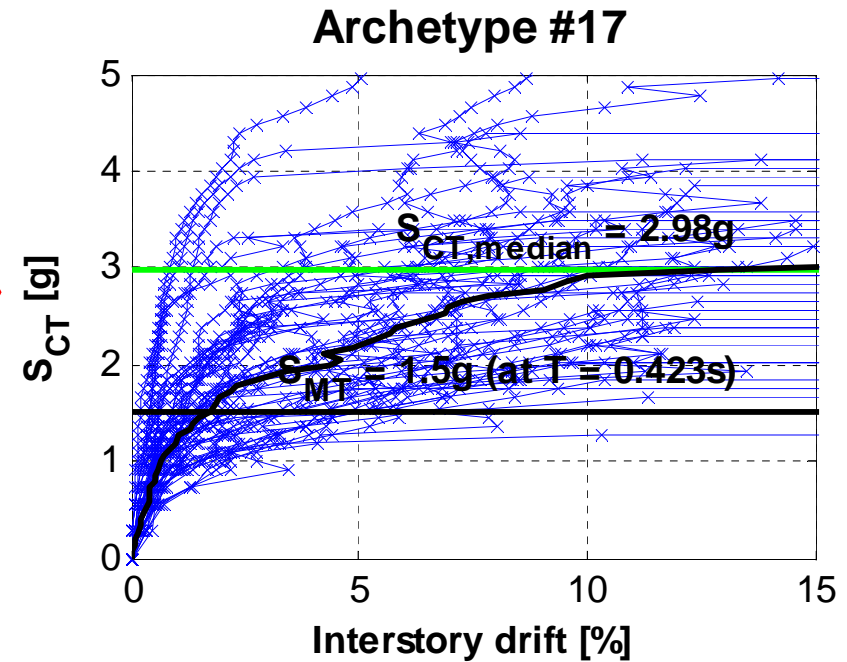
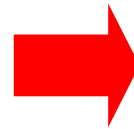
b) scaled at $T_{model} = 0.495$ s

Further observations

- Effect of 'scaling' fundamental period



a) scaled at $T_{upper} = 0.604$ s



b) scaled at $T_{model} = 0.423$ s

Further observations

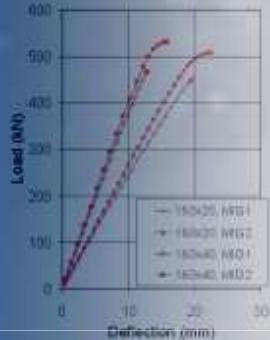
- Model parameter sensitivity

- capping displ. 50 \rightarrow 75 mm
capping slope -0.15 \rightarrow -0.05 +6%

- α_p 0.75 \rightarrow 0.40
 β_p 0.25 \rightarrow 0.21 +8%

- adjusted initial stiffness +6%

- 1.4 x strength +30%



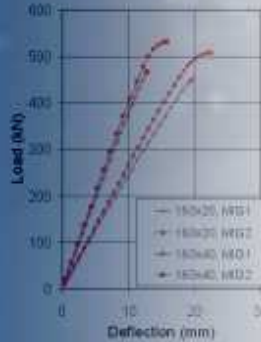
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Performance quantification

- check

R = 4 High seismic (SDC Dmax)
 $S_S = 1.5, S_1 = 0.9 (S_{DS} = 1.0, S_{D1} = 0.6)$



Archetype	Story #	Function	Ω_0 [-]	μ_c [-]	SSF [-]	S_{MT} (T_{upper}) [g]	SF_{anchor} [-]	β_{tot} [-]	\hat{S}_{CT} [g]	CMR [-]	ACMR [-]	
1	1	Commercial	2.38	6.25	1.31	1.50	2.1	0.70	2.79	1.86	2.44	>
5	2	Commercial	2.40	4.37	1.26	1.50	1.89	0.70	3.06	2.04	2.57	>
9	3	Commercial	2.39	3.36	1.22	1.50	1.98	0.70	2.88	1.92	2.34	>
Mean											2.45	>

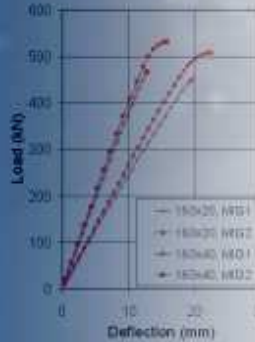
2	1	1&2 Family	9.91	6.31	1.31	1.50	2.1	0.70	6.00	4.00	5.24	>
6	2	1&2 Family	4.91	4.95	1.27	1.50	1.89	0.70	4.63	3.09	3.92	>
10	3	Multi-Family	2.52	4.06	1.25	1.50	1.98	0.70	3.16	2.11	2.64	>
13	4	Multi-Family	2.56	3.00	1.20	1.50	2	0.70	2.94	1.96	2.35	>
15	5	Multi-Family	2.57	2.72	1.20	1.50	2.1	0.70	2.93	1.96	2.35	>
Mean											3.30	>

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Performance quantification

- even for taller buildings

R = 4 High seismic (SDC Dmax)
 $S_S = 1.5, S_1 = 0.9 (S_{DS} = 1.0, S_{D1} = 0.6)$



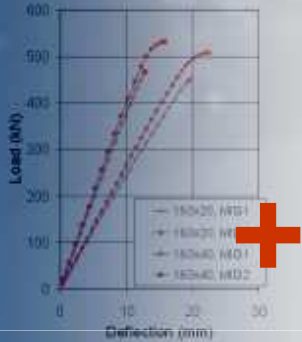
Archetype	Story #	Function	Ω_0 [-]	μ_c [-]	SSF [-]	S_{MT} (T_{upper}) [g]	SF_{anchor} [-]	β_{tot} [-]	\hat{S}_{CT} [g]
2	1	1&2 Family	9.91	6.31	1.31	1.50	2.1	0.70	6.00
6	2	1&2 Family	4.91	4.95	1.27	1.50	1.89	0.70	4.63
10	3	Multi-Family	2.52	4.06	1.25	1.50	1.98	0.70	3.16
13	4	Multi-Family	2.56	3.00	1.20	1.50	2	0.70	2.94
15	5	Multi-Family	2.57	2.72	1.20	1.50	2.1	0.70	2.93
17	6	Multi-Family	2.57	2.48	1.22	1.49	2.49	0.70	2.45
18	7	Multi-Family	2.08	2.40	1.22	1.33	2.37	0.70	2.54
19	8	Multi-Family	2.34	2.34	1.22	1.20	2.46	0.70	2.43
21	10	Multi-Family	2.42	2.31	1.23	1.02	2.49	0.70	2.25

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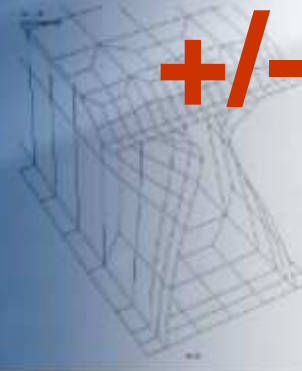


Performance quantification

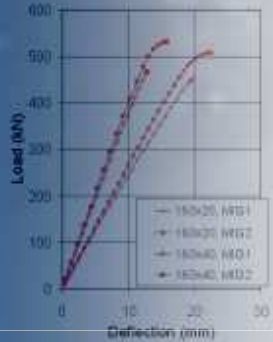
- $R = 4 !$
- results and component behavior are very similar to wooden shear wall – as good as wood
- $R = 6$ is in code for wooden shear wall
- additional finishing, partition walls?
- short period bldgs!
- ASD design strength derivation from test
- uncertainties in the monotonic backbone estimation



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Performance quantification



conventional R factor vs. ATC-63

?

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Thank you for your attention!

But don't go anywhere...

